Low Complexity Precoding and Detection in Multi-User Massive MIMO OTFS Downlink

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Abstract—We consider the problem of degradation in performance of multi-carrier multi-user massive MIMO systems when channel induced Doppler spread is high. Recently, Orthogonal Time Frequency Space (OTFS) modulation has been shown to be robust to channel induced Doppler spread. In OTFS based systems, information symbols are embedded in the delay-Doppler (DD) domain where they are jointly modulated to generate the time-domain transmit signal. Due to the multi-path delay and Doppler shifts, the DD domain information symbols need to be jointly demodulated at the receiver. For multi-carrier based communication (e.g., Orthogonal Frequency Division Multiplexing (OFDM)), massive MIMO systems have been shown to achieve high spectral and energy efficiency with low complexity multi-user precoding in the downlink. Extending the same to OTFS based downlink multi-user massive MIMO systems is challenging due to the requirement for joint demodulation of all information symbols at the user terminal (UT). In this paper, we solve this problem by proposing a novel OTFS based multi-user precoder at the base station (BS) and a corresponding low complexity detector (LCD) at the user terminals (UTs), which allows for separate demodulation of each DD domain information symbol at the UT. The complexity of the proposed precoder increases only linearly with increasing number of BS antennas Q and the number of UTs. We show, through analysis, that as Q increases (with total transmitted power decreased linearly with Q), the proposed low complexity detector achieves a sum spectral efficiency close to that achieved with optimal joint demodulation at each UT. Numerical simulations confirm our analysis and also show that the spectral efficiency and error rate performance of the proposed OTFS based massive MIMO precoder (with the proposed LCD detector at each UT) is significantly more robust to channel induced Doppler spread when compared to OFDM based multi-user massive MIMO systems.

Index Terms—Doppler spread, massive MIMO, multi-user, OTFS, precoder.

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I. INTRODUCTION

N THIS paper, we consider low complexity precoding and detection for downlink massive MIMO systems where information is embedded in the Delay-Doppler (DD) domain. Recently, Orthogonal Time Frequency Space (OTFS) modulation has been introduced, where information is embedded in the DD domain [1]–[3]. This improves robustness towards channel induced Doppler spread which is otherwise known to severely degrade the performance of multi-carrier systems (e.g., Orthogonal Frequency Division Multiplexing (OFDM)) where information is embedded in the Time-Frequency (TF) domain [1], [4].

In OTFS modulation, DD domain information symbols interfere with each other due to the channel induced delay and Doppler shifts, and therefore they need to be jointly demodulated at the receiver. This can be challenging in the downlink where the UTs are receivers. Towards this end, [5]-[7], [8] have considered low-complexity message passing (MP) based detectors which have good error rate performance when the DD domain channel is sparse i.e., small number of channel paths. However, in rich scattering environments with a large number of channel multi-paths, the performance of MP based detector degrades. In [9], a Linear Minimum Mean Squared Error (LMMSE) estimator based OTFS detector has been proposed whose complexity increases with increasing delay and Doppler spread. In [10], a point-to-point MIMO-OTFS system has been considered for high Doppler spread channels, for which a Markov Chain Monte Carlo (MCMC) sampling based detector has been proposed. However, the complexity of this MCMC based detector is $O(M^3 N^3)$ where M and N are the number of sub-divisions of the delay and Doppler domain respectively. The complexity of this MCMC detector can be prohibitive for large (M, N). A low-complexity Linear MMSE detector has also been proposed in [11] having complexity $O(M^2 N^2 P)$ (P is the number of channel multi-paths), though this complexity can still be high for OTFS systems where (M, N) is large. In [12], low complexity OTFS detection based on a variational Bayes approach is proposed having overall complexity $O(MNP) + O(MN\log(MN)).$

Next generation communication systems are expected to achieve higher throughput and reliability at much higher mobile speed when compared to Fourth Generation systems [13]. As next generation systems are expected to operate in higher frequency bands, achieving high throughput at high mobile speed is a challenge due to increased channel induced Doppler spread. Massive MIMO systems based on large antenna arrays at the base station (BS) have been proposed for improving the spectral and energy efficiency of multi-user cellular wireless communication systems [14]. However, to the best of our knowledge there

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is no work done so far on *large antenna array* based *DD domain multi-user downlink precoding* for massive MIMO systems.

Recently in [15], the authors have proposed a large-antenna array based low-complexity receiver for decoding the downlink OTFS signal transmitted from a single-antenna BS. However, the authors ignore inter-carrier interference (ICI) and inter-symbol interference (ISI) as they assume ideal pulse shaping transmit and receiver waveforms which satisfy the bi-orthogonality condition (see equation (17) in [15]). Such ideal pulses however do not exist. Further, the Doppler shift of each channel path is assumed to be an integer multiple of the Doppler resolution in the DD domain, and therefore interference due to fractional Doppler has also been ignored in [15]. Also, in [15], only a single user scenario is considered with no precoding at the BS as only single-antenna BS transmission is considered. In [16], a path division multiple access OTFS massive MIMO system has been proposed where the angle domain is used to separate the uplink signal from different UTs. This method however assumes precise knowledge of the antenna steering vector at the BS and also accurate knowledge of the angle of arrivals from the UTs.

In [17], OTFS modulation based single user massive MIMO beamforming is proposed. OTFS modulation transforms the information symbols into TF domain symbols on which beamforming is performed. Due to OTFS modulation, each information symbol is spread over the entire TF domain and therefore at the receiver, a linear MMSE estimator based interference cancellation detector is used. For each information symbol, the complexity of the linear MMSE based detection is at least O(MN). Since there are MN information symbols in an OTFS frame, the total detection complexity is at least $O(M^2 N^2)$.

In this paper, we consider a *multi-user* massive MIMO downlink OTFS system where a BS having a *large* uniform rectangular antenna array (URA) with $Q=Q_hQ_v$ antennas (Q_h rows and Q_v columns) serves K user terminals (UTs) each having a single antenna. We consider practical non-ideal pulse shaping and fractional Doppler which results in ICI, ISI and Doppler interference, due to which the effective DD domain channel matrices between the BS and the UTs are not as sparse as that when ideal pulses and integral Doppler is assumed. In such a scenario, multi-antenna information precoding in the DD domain can have very high complexity since all KMN information symbols have to be jointly precoded and transmitted from the Q BS antennas. There is therefore a need to design *low complexity* multi-user precoding and detection methods for massive MIMO OTFS systems. Specific contributions of our paper are:

- 1) With rectangular pulse shaping and fractional Doppler, in Section IV we propose a low-complexity DD domain based multi-user precoder for massive MIMO OTFS systems where perfect channel state information (CSI) of all UTs is available at the BS. The precoding complexity is $O(QMN^2\sum_{s=1}^K L_s)$ where L_s is the number of channel paths between the BS and the s-th UT. Note that the complexity increases only *linearly* with the number of BS antennas Q and the number of UTs K.
- 2) With this proposed multi-user precoder, the optimal detector at each UT has prohibitive complexity as it jointly decodes all the MN DD domain information symbols in an OTFS frame. Therefore, in Section V we propose a low complexity DD domain detector (LCD) at the UT, which performs separate detection for each information symbol and therefore has lower complexity than the optimal detector. Due to separate detection of each information

- symbol, the LCD detector along with the TF to DD domain converter has only a $O(MN \log(MN))$ complexity, which is independent of the amount of delay/Doppler spread and the number of channel paths.
- 3) In Section V, we also derive an expression for the achievable sum spectral efficiency (SE) with the proposed low complexity detector. Analysis of this expression reveals that as the number of BS antennas becomes large (with total transmitted power reduced linearly with increasing *Q*), the sum SE achieved by the proposed LCD detector is close to that achieved by the optimal detector.
- 4) Analysis reveals that in the large antenna regime, the SE of the proposed LCD detector is limited only by AWGN and is almost independent of multi-user and inter-symbol interference. This is similar to the effect of vanishing multi-user and inter-symbol interference in Time-Frequency domain based massive MIMO systems where linear precoders are used [18].
- 5) Numerical simulations confirm that, in the large antenna regime, the proposed LCD detector achieves sum SE close to that achieved by the optimal detector. Through numerical simulations, we also compare the sum SE achieved by the proposed multi-user precoder and LCD detector with that achieved by OFDM massive MIMO systems based on Maximum Ratio Transmission (MRT) multi-user precoding [18]. These simulations reveal that the proposed DD domain based multi-user massive MIMO precoding and LCD detection achieves *significantly better* SE than OFDM massive MIMO systems in channels where Doppler shift is high.
- 6) In Section VI-A, we compare the coded error rate performance of OTFS and OFDM downlink massive MIMO systems when the BS has *imperfect* channel state information (CSI). Simulations reveal that indeed the proposed low-complexity OTFS precoder with the LCD detector achieves significantly better coded error rate performance than OFDM massive MIMO with much less channel estimation overhead.

Notations: For integers x and M, $[x]_M$ denotes the smallest non-negative integer congruent to x modulo M. For any real y, [y] is the greatest integer less than or equal to y. The zero mean circular symmetric complex Gaussian distribution having variance N_0 is denoted by $\mathcal{CN}(0,N_0)$. For any square matrix \mathbf{A} , $\mathrm{Tr}(\mathbf{A})$ and $|\mathbf{A}|$ denote the trace and determinant of \mathbf{A} , respectively. $\mathrm{Diag}(a_1,a_2,\ldots,a_n)$ denotes a square $n\times n$ diagonal matrix whose element in the i-th row and i-th column is $a_i, i=1,2,\ldots,n$.

II. SYSTEM MODEL

We consider the downlink of an OTFS based multi-user massive MIMO system with Q co-located antennas at the base station (BS) and a single antenna at each of the K user terminals (UTs). The antenna array at the BS is in the form of a Uniform Rectangular Array (URA) with distance d between adjacent antenna elements. The number of rows and columns of antenna elements in the URA are Q_v and Q_h respectively, i.e., $Q=Q_hQ_v$. The Delay-Doppler channel between the q-th BS antenna and the s-th UT is given by [19], [20]

$$h_{q,s}(\tau,\nu) = \sum_{i=1}^{L_s} h_{q,s,i} \, \delta(\tau - \tau_{s,i}) \, \delta(\nu - \nu_{s,i}) ,$$

$$s = 1, 2, \dots, K, \quad q = 1, 2, \dots, Q$$
 (1)

where L_s denotes the number of channel paths between the BS and the s-th UT. Further, $\tau_{s,i}$ and $\nu_{s,i}$ are the delay and Doppler along the i-th path $(i=1,2,\ldots,L_s)$ between the BS and the s-th UT. In (1), $\delta(\cdot)$ is the impulse function. Further, $h_{q,s,i}$ is the complex channel gain between the q-th BS antenna and the s-th UT along the i-th path and is given by [21]

$$h_{q,s,i} = g_{s,i} e^{j\frac{2\pi d}{\lambda} \left([q-1]_{Q_h} \sin \phi_{s,i} \sin \theta_{s,i} + \left\lfloor \frac{q-1}{Q_h} \right\rfloor \cos \theta_{s,i} \right)},$$

$$q = 1, 2, \dots, Q, s = 1, 2, \dots, K, i = 1, 2, \dots, L_s \quad (2)$$

where $g_{s,i}$ models the complex channel gain of the i-th path, i.e., $g_{s,i}$ are i.i.d. $\mathcal{CN}(0,\beta_{s,i}),\ s=1,2,\ldots,K$, $i=1,2,\ldots,L_s$. Further, let the vector of channel path gains between the s-th UT and the BS be denoted by

$$\mathbf{g}_{s} \stackrel{\Delta}{=} (g_{s,1}, g_{s,2}, \cdots, g_{s,L_{s}})^{T}, s = 1, 2, \dots, K.$$
 (3)

In (2), $\theta_{s,i}$ and $\phi_{s,i}$ are respectively the zenith and azimuthal angles of departure for the *i*-th channel path from the BS to the *s*-th UT.¹ Also, λ is the wavelength of the carrier.

In this paper we consider coding across several OTFS frames which are sequential in time. The zenith and azimuthal angles of departure, the Doppler shift, delay and channel gain for each path are assumed to be fixed for the entire duration of a codeword. As an example, with OTFS frames of duration 0.25 milliseconds (ms) and a codeword spanning hundred OTFS frames, the total duration of the codeword is 25 ms. With a bandwidth of 5 MHz, the resolution of the delay domain is $1/(5\text{MHz}) = 0.2\mu s$. The delay of a channel path can change by an order of $0.2\mu s$ if and only if the UT travels a distance of roughly 60 m (i.e., distance travelled in $0.2\mu s$ at speed of light). Even for a UT with a mobile speed of 360 Km/hr (i.e., 100 m/s), it would take 600 ms for this to happen, which is much greater than the 25 ms duration of a codeword. In this paper, we therefore assume the zenith and azimuthal angles of departure, the Doppler shift, delay and channel gain for each path to be fixed for a few tens of ms, i.e., the entire duration of the codeword. Subsequently, these parameters which are fixed for the entire codeword duration, are denoted by

$$\mathcal{P} \stackrel{\Delta}{=} \left\{ \{L_s\}_{s=1}^K, \{\theta_{s,i}, \phi_{s,i}, \tau_{s,i}, \nu_{s,i}, g_{s,i}\}_{s=1,i=1}^{K,L_s} \right\}. \tag{4}$$

Let $x_q(t)$ denote the time-domain signal transmitted from the q-th BS antenna. The time-domain signal received at the s-th UT is given by [20]

$$y_s(t) = \sum_{q=1}^{Q} \int \int h_{q,s}(\tau,\nu) x_q(t-\tau) e^{j2\pi\nu(t-\tau)} d\tau \, d\nu + \tilde{w}_s(t)$$

$$\stackrel{(a)}{=} \sum_{q=1}^{Q} \sum_{i=1}^{L_s} h_{q,s,i} \, x_q(t - \tau_{s,i}) \, e^{j2\pi\nu_{s,i}(t - \tau_{s,i})} \, + \, \tilde{w}_s(t) \tag{5}$$

where $\tilde{w}_s(t)$ is the additive white Gaussian noise (AWGN) at the s-th UT and step (a) follows from (1). The multi-user massive MIMO downlink system is depicted in Fig. 1.

 1We assume that for any two channel paths to a UT, both the corresponding zenith and azimuthal angles are not equal. That is, for all $s=1,2,\ldots,K$ and any $i\neq k, (\theta_{s,i}\phi_{s,i})\neq (\theta_{s,k},\phi_{s,k}),$ i.e., $\theta_{s,i}=\theta_{s,k}$ and $\phi_{s,i}=\phi_{s,k}$ if and only if i=k. In practical scenarios, due to randomly distributed scatterers, two UTs may have the same zenith and azimuthal angles for some paths between the BS and these UTs. However, in this paper we consider that the BS schedules any two such UTs onto different physical resource, in order that they do not interfere with each other. Therefore, in this paper we propose joint DD domain precoding only for those UTs for which, the zenith and the azimuthal angles for any channel paths to these UTs are not both equal, i.e., for any $s\neq s'$ and all $i=1,2,\ldots,L_s,k=1,2,\ldots,L_{s'},(\theta_{s,i},\phi_{s,i})\neq (\theta_{s',k},\phi_{s',k})$.

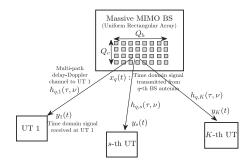


Fig. 1. A multi-user massive MIMO downlink system.

III. OTFS MODULATION AND DEMODULATION

The DD domain is T seconds wide along the delay domain and $\Delta f = 1/T$ Hz wide along the Doppler domain. The delay domain is further sub-divided into M equal sub-divisions each T/M seconds wide. Similarly the Doppler domain is sub-divided into N equal sub-divisions each $\Delta f/N$ Hz wide. The combination of a sub-division along the delay domain and a sub-division along the Doppler domain is referred to as a Delay Doppler Resource Element (DDRE). There are therefore MN DDREs in one OTFS frame and each DDRE carries one information symbol. Each DDRE is denoted by its index $k=0,1,\ldots,N-1$ along the Doppler domain and its index $l=0,1,\ldots,M-1$ along the delay domain.

At the q-th BS antenna, the DD domain transmit symbols $x_q[k,l], k=0,1,\ldots,N-1, l=0,1,\ldots,M-1$ are converted to the time-domain signal $x_q(t)$ using OTFS modulation [1]. At the UT, the received time-domain signal y(t) is transformed back to the DD domain using OTFS demodulation. For OTFS modulation, the DD domain signal $x_q[k,l]$ is first transformed to the Time-Frequency (TF) domain signal $X_q[n,m]$ using the Inverse Symplectic Finite Fourier Transform (ISFFT), i.e.

$$X_{q}[n,m] = \frac{1}{\sqrt{MN}} \sum_{k=0}^{N-1} \sum_{l=0}^{M-1} x_{q}[k,l] e^{j2\pi \left(\frac{nk}{N} - \frac{ml}{M}\right)}$$

$$n = 0, 1, \dots, N-1, \ m = 0, 1, \dots, M-1.$$
 (6)

Next, $X_q[n,m]$ is then transformed to the time-domain signal $\tilde{x}_q(t)$ using the Heisenberg transform²

$$\tilde{x}_q(t) = \sum_{n=0}^{N-1} \sum_{m=0}^{M-1} X_q[n, m] g_{tx}(t - nT) e^{j2\pi m\Delta f(t - nT)}$$
 (7)

where the transmit pulse $g_{tx}(\cdot)$ is rectangular and is given by

$$g_{tx}(t) \stackrel{\Delta}{=} \begin{cases} \frac{1}{\sqrt{T}} & \text{, if } 0 \le t < T \\ 0 & \text{, otherwise.} \end{cases}$$
 (8)

 2 Transformation of the TF signal $X_q[n,m]$ to the time-domain can also be performed using the Inverse Fourier Transform as considered in [16], [22], [23] However, the use of the Inverse Fourier Transform requires a Cyclic-Prefix (CP) for each $n=0,1,\ldots,N-1$, i.e., N CPs in each OTFS frame. In [24] it has been shown that using the Heisenberg transformation (instead of the Inverse Fourier Transform) requires only one CP for the entire OTFS frame without any performance penalty, i.e., the CP overhead is significantly less when using the Heisenberg transformation.

A CP of duration equal to the maximum channel path delay, i.e.³

$$\tau_{max} \stackrel{\Delta}{=} \max_{\substack{s=1,2,\dots,K\\i=1,2,\dots,L_s}} \tau_{s,i} \tag{9}$$

is appended to $\tilde{x}_q(t)$ resulting in the time-domain signal $x_q(t)$ to be transmitted from the q-th BS antenna, i.e.

$$x_{q}(t) = \begin{cases} \sum_{n=-1}^{N-1} \sum_{m=0}^{M-1} X_{q}[[n]_{N}, m] g_{tx}(t - nT) e^{j2\pi m\Delta f(t - nT)}, \\ -\tau_{max} \le t < NT \\ 0, t < -\tau_{max} \text{ and } t \ge NT. \end{cases}$$

In (10), the TF symbol $X_q[n,m], n \geq 0$ contributes to the overall transmit signal $x_q(t)$ only through the term $X_q[n,m]g_{tx}(t-nT)\,e^{j2\pi m\Delta f(t-nT)}$ and therefore since $g_{tx}(\cdot)$ is time-limited to the interval [0,T), it follows that this term is limited to the interval [nT,(n+1)T) along the time-domain and roughly along the interval $[m\Delta f,(m+1)\Delta f]$ along the frequency domain $([nT,(n+1)T)\times[m\Delta f,(m+1)\Delta f]$ is referred to as the (m,n)-th time-frequency resource element (TFRE)). In the R.H.S. of (10), the summation term due to n=-1 corresponds to the CP and we limit it to the time-interval $[-\tau_{max},0)$. Since $m=0,1,\ldots,(M-1)$ and $n=-1,0,1,\ldots,(N-1)$, the transmit signal $x_q(t)$ is therefore time-limited to the interval $[-\tau_{max},NT)$ and has a bandwidth of $M\Delta f$ Hz. For OTFS demodulation at the s-th UT, the received time-domain signal $y_s(t)$ is first transformed to the TF domain using the Wigner transform [1] i.e.

$$Y_s[n,m] = \int_0^{NT} g_{rx}^*(t-nT) y_s(t) e^{-j2\pi m\Delta f(t-nT)} dt$$

$$n = 0, 1, \dots, N-1, m = 0, 1, \dots, M-1$$
 (11)

where $g_{rx}(\cdot)$ is the receive pulse which we take to be rectangular i.e., $g_{rx}(t) = g_{tx}(t)$. The TF domain signal is then transformed back to the DD domain using SFFT i.e.,

$$\widehat{x}_s[k,l] = \frac{1}{\sqrt{MN}} \sum_{n=0}^{N-1} \sum_{m=0}^{M-1} Y_s[n,m] e^{-j2\pi \left(\frac{nk}{N} - \frac{ml}{M}\right)}$$

$$k = 0, 1, \dots, N-1, \ l = 0, 1, \dots, M-1. \tag{12}$$

Let $\hat{\mathbf{x}}_s \in \mathbb{C}^{MN \times 1}$ denote the vector of these received DD domain symbols at the s-th UT as given by (13), as shown at the bottom of this page.

From Appendix A in this paper and [5], it follows that⁴

$$\widehat{\mathbf{x}}_s = \sum_{q=1}^{Q} \mathbf{H}_{q,s} \, \mathbf{x}_q + \mathbf{w}_s \tag{14}$$

where $\mathbf{x}_q \in \mathbb{C}^{MN \times 1}$ is the vector of DD domain symbols to be transmitted from the q-th BS antenna, and is given by (13). In (14), \mathbf{w}_s is the vector of i.i.d. $\mathcal{CN}(0,N_0)$ additive noise samples in the DD domain and is given by (13). In (13), $w_s[k,l]$ is the received noise sample at the s-th UT in the (k,l)-th DDRE and is given by (35) in Appendix A. The matrix $\mathbf{H}_{q,s} \in \mathbb{C}^{MN \times MN}$ is the effective DD domain channel between the s-th UT and the q-th BS antenna and is given by

$$\mathbf{H}_{q,s} \stackrel{\Delta}{=} \sum_{i=1}^{L_s} h_{q,s,i} \, \mathbf{A}_{s,i} \tag{15}$$

where the matrix $\mathbf{A}_{s,i} \in \mathbb{C}^{MN \times MN}$ scaled by $h_{q,s,i}$ is the contribution of the i-th channel path of the s-th UT to the DD domain channel matrix $\mathbf{H}_{q,s}$ between the q-th BS antenna and the s-th UT (see the derivation of (14) and (15) in Appendix A). The entry of $\mathbf{A}_{s,i}$ in its (kM+l+1)-th row and (k'M+l'+1)-th column is given by $a_{s,i,k,l}[k',l']$ in (39) of Appendix A.

IV. PROPOSED MULTI-USER DOWNLINK PRECODING IN DD DOMAIN

Let $u_s[k,l] \sim \mathcal{CN}(0,1)$, $k=0,1,\ldots,N-1,l=0,1,\ldots,M-1$ denote the i.i.d. DD domain information symbols to be communicated to the s-th UT on the (k,l)-th DDRE. Also, let $\mathbf{u}_s \in \mathbb{C}^{MN \times 1}$ denote the vector of all MN information symbols for the s-th UT, which is given by (16), as shown at the bottom of this page. Assuming perfect knowledge of the effective DD domain channel matrices $\mathbf{H}_{q,s}$, $q=1,2,\ldots,Q$, $s=1,2,\ldots,K$ at the BS, in the following we propose to precode \mathbf{u}_s into the DD domain transmit signal vectors \mathbf{x}_q , $q=1,2,\ldots,Q$, i.e.

$$\mathbf{x}_{q} = \sqrt{\frac{E_{T}}{\eta}} \sum_{s=1}^{K} \mathbf{H}_{q,s}^{H} \mathbf{u}_{s}, \, \eta \stackrel{\Delta}{=} QMN \sum_{s=1}^{K} \sum_{i=1}^{L_{s}} \beta_{s,i}. \quad (17)$$

In (17), the DD domain signal \mathbf{x}_q transmitted from the q-th BS antenna depends on the DD domain channel matrices $\mathbf{H}_{q,s}, s = 1, 2, \ldots, K$ between the UTs and the q-th BS antenna. Further, from (15) we know that $\mathbf{H}_{q,s}$ depends on $h_{q,s,i}$ which in turn depends on the zenith and azimuthal angles of departure between the BS and the s-th UT. Therefore, the proposed precoder in (17) incorporates spatial precoding. Later in Section V, we show that with a large BS antenna array, this precoder allows

⁴Note that, just as in [5] we consider the path delays $\tau_{s,i}, i=1,2,\ldots,L_s$ to be integer multiples of $T/M=1/(M\Delta f)$ since the sampling time duration $1/(M\Delta f)$ is small for wide bandwidth systems and therefore it suffices to approximate the path delay with its nearest integer multiple of $1/(M\Delta f)$ [25]. Therefore, $l_{\mathcal{T}_{s,i}} \stackrel{\Delta}{=} \tau_{s,i} M\Delta f$ is an integer.

$$\widehat{\mathbf{x}}_{s} \stackrel{\triangle}{=} (\widehat{x}_{s}[0,0], \dots, \widehat{x}_{s}[0,M-1], \widehat{x}_{s}[1,0], \dots, \widehat{x}_{s}[1,M-1], \dots, \widehat{x}_{s}[N-1,0], \dots, \widehat{x}_{s}[N-1,M-1])^{T},
\mathbf{x}_{q} \stackrel{\triangle}{=} (x_{q}[0,0], \dots, x_{q}[0,M-1], x_{q}[1,0], \dots, x_{q}[1,M-1], \dots, x_{q}[N-1,0], \dots, x_{q}[N-1,M-1])^{T},
\mathbf{w}_{s} \stackrel{\triangle}{=} (w_{s}[0,0], \dots, w_{s}[0,M-1], w_{s}[1,0], \dots, w_{s}[1,M-1], \dots, w_{s}[N-1,0], \dots, w_{s}[N-1,M-1])^{T}$$
(13)

$$\mathbf{u}_s \stackrel{\Delta}{=} (u_s[0,0], \dots, u_s[0,M-1], u_s[1,0], \dots, u_s[1,M-1], \dots, u_s[N-1,0], \dots, u_s[N-1,M-1])^T$$
(16)

³The CP helps in avoiding interference between OTFS frames transmitted one after the other in the time-domain.

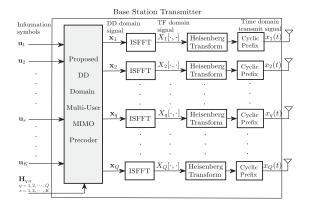


Fig. 2. Block diagram of the BS downlink transmitter with the proposed OTFS Multi-user Massive MIMO Precoder.

for separate detection of each DD domain information symbol (i.e., low complexity detection), as it results in vanishingly small inter-symbol and multi-user interference at each UT. The complete block diagram of the downlink transmitter at the BS is shown in Fig. 2 (the operations in (17) are implemented in the shaded block).

We note that the proposed precoder in (17) is different from the OTFS modulation based single user massive MIMO beamforming proposed in [17]. This is because, in (17) we perform spatial precoding in the DD domain whereas in [17] single-user beamforming is performed only in the TF domain. As we shall see later in Section V, the proposed precoder allows for separate DD domain detection of each information symbol which has a complexity of only $O(MN\log(MN))$ when compared to the detection complexity of at least $O(M^2 N^2)$ in [17]. The average transmitted energy is given by

$$\mathbb{E}_{\mathbf{u}_{s},\mathbf{g}_{s}} \left[\sum_{q=1}^{Q} \int_{-\tau_{max}}^{NT} |x_{q}(t)|^{2} dt \right]$$

$$= \mathbb{E}_{\mathbf{u}_{s},\mathbf{g}_{s}} \left[\sum_{q=1}^{Q} \int_{0}^{NT} |x_{q}(t)|^{2} dt \right]$$

$$+ \mathbb{E}_{\mathbf{u}_{s},\mathbf{g}_{s}} \left[\sum_{q=1}^{Q} \int_{-\tau_{max}}^{0} |x_{q}(t)|^{2} dt \right]$$
(18)

where the expectation is w.r.t. $\mathbf{u}_s, \mathbf{g}_s, s = 1, 2, \dots, K$ (see (3)). From (6), (8) and (10) it follows that

$$\mathbb{E}_{\mathbf{u}_{s},\mathbf{g}_{s}} \left[\sum_{q=1}^{Q} \int_{0}^{NT} |x_{q}(t)|^{2} dt \right]$$

$$= \mathbb{E}_{\mathbf{u}_{s},\mathbf{g}_{s}} \left[\sum_{q=1}^{Q} \sum_{n=0}^{N-1} \sum_{m=0}^{M-1} |X_{q}[n,m]|^{2} \right]$$

$$= \mathbb{E}_{\mathbf{u}_{s},\mathbf{g}_{s}} \left[\sum_{q=1}^{Q} \sum_{k=0}^{N-1} \sum_{l=0}^{M-1} |x_{q}[k,l]|^{2} \right]$$

$$= \sum_{q=1}^{Q} \mathbb{E}_{\mathbf{u}_{s},\mathbf{g}_{s}} \left[\|\mathbf{x}_{q}\|^{2} \right]$$

$$(19)$$

where the precoded DD domain symbol vector \mathbf{x}_q is given by (17). From (17) it is clear that

$$\sum_{q=1}^{Q} \mathbb{E}_{\mathbf{u}_{s},\mathbf{g}_{s}} \left[\|\mathbf{x}_{q}\|^{2} \right] = \sum_{q=1}^{Q} \operatorname{Tr} \left(\mathbb{E}_{\mathbf{u}_{s},\mathbf{g}_{s}} \left[\mathbf{x}_{q} \mathbf{x}_{q}^{H} \right] \right)$$

$$\stackrel{(a)}{=} \frac{E_{T}}{\eta} \sum_{q=1}^{Q} \sum_{s=1}^{K} \operatorname{Tr} \left(\mathbb{E}_{\mathbf{g}_{s}} \left[\mathbf{H}_{q,s}^{H} \mathbf{H}_{q,s} \right] \right)$$

$$\stackrel{(b)}{=} \frac{E_{T}}{\eta} \sum_{q=1}^{Q} \sum_{s=1}^{K} \sum_{i_{1}=1}^{L_{s}} \sum_{i_{2}=1}^{L_{s}}$$

$$\mathbb{E}_{\mathbf{g}_{s}} \left[h_{q,s,i_{1}}^{*} h_{q,s,i_{2}} \right] \operatorname{Tr} \left(\mathbf{A}_{s,i_{1}}^{H} \mathbf{A}_{s,i_{2}} \right)$$

$$\stackrel{(c)}{=} \frac{MNE_{T}}{\eta} \sum_{q=1}^{Q} \sum_{s=1}^{K} \sum_{i=1}^{L_{s}} \mathbb{E}_{\mathbf{g}_{s}} \left[|g_{s,i}|^{2} \right]$$

$$= E_{T} \frac{QMN \sum_{s=1}^{K} \sum_{i=1}^{L_{s}} \beta_{s,i}}{\eta} = E_{T} \quad (20)$$

where step (a) follows from the fact that $u_s[k,l] \sim \text{i.i.d.}\,\mathcal{CN}(0,1)$. Step (b) follows from the R.H.S. of (15). Step (c) follows from the expression for $h_{q,s,i}$ in (2) and the fact that $g_{s,i}, s=1,2,\ldots,K, i=1,2,\ldots,L_s$ are i.i.d. We have also used the fact that $\mathbf{A}_{s,i}^H\mathbf{A}_{s,i}=\mathbf{I}$ (see (42)). The last step follows from the definition of η in (17). Similarly, from (2), (6), (8), (10), (15) and (17) it can be shown that

$$\mathbb{E}_{\mathbf{u}_s,\mathbf{g}_s} \left[\sum_{q=1}^{Q} \int_{-\tau_{max}}^{0} |x_q(t)|^2 dt \right] = E_T \frac{\tau_{max}}{NT}$$
 (21)

and therefore using (19), (20) and (21) in (18), we get

$$\mathbb{E}_{\mathbf{u}_s,\mathbf{g}_s} \left[\sum_{q=1}^{Q} \int_{-\tau_{max}}^{NT} |x_q(t)|^2 dt \right] = E_T \left(1 + \frac{\tau_{max}}{NT} \right). \quad (22)$$

The proposed precoder in (17) involves matrix multiplications $(\mathbf{H}_{q,s}^H\mathbf{u}_s, s=1,2,\ldots,K)$ for generating the DD domain transmit signal at each BS antenna. In Appendix A, from the second equation in (39) it is clear that each column of $\mathbf{A}_{s,i}$ has only N non-zero elements out of MN elements. From (15) it then follows that each column of $\mathbf{H}_{q,s}$ has at most NL_s non-zero elements. Hence the complexity of the proposed precoder is $O(QMN^2\sum_{s=1}^KL_s)$ for each OTFS frame, i.e., the precoding complexity increases only *linearly* with the number of BS antennas Q and the number of UTs K.

Using (17) in (14), the received vector of DD domain symbols at the s-th UT is

$$\widehat{\mathbf{x}}_{s} = \sum_{q=1}^{Q} \mathbf{H}_{q,s} \left(\sqrt{\frac{E_{T}}{\eta}} \sum_{s'=1}^{K} \mathbf{H}_{q,s'}^{H} \mathbf{u}_{s'} \right) + \mathbf{w}_{s}$$

$$= \sqrt{\frac{E_{T}}{\eta}} \mathbf{G}_{s,s} \mathbf{u}_{s} + \sqrt{\frac{E_{T}}{\eta}} \sum_{\substack{s'=1\\s'\neq s}}^{K} \mathbf{G}_{s,s'} \mathbf{u}_{s'} + \mathbf{w}_{s},$$

$$\mathbf{G}_{s,s'} \stackrel{\Delta}{=} \sum_{q=1}^{Q} \mathbf{H}_{q,s} \mathbf{H}_{q,s'}^{H}.$$
(23)

Using (15) in (23) we get

$$\mathbf{G}_{s,s'} = \sum_{q=1}^{Q} \mathbf{H}_{q,s} \, \mathbf{H}_{q,s'}^{H} = \sum_{q=1}^{Q} \sum_{i=1}^{L_s} \sum_{k=1}^{L_{s'}} h_{q,s,i} h_{q,s',k}^* \mathbf{A}_{s,i} \mathbf{A}_{s',k}^{H}.$$
(24)

In (23), the relation between the transmitted information symbol vector \mathbf{u}_s and the received DD domain signal vector $\widehat{\mathbf{x}}_s$ is similar to that of a $MN \times MN$ MIMO system, for which the largest information rate (i.e., $I(\widehat{\mathbf{x}}_s;\mathbf{u}_s)$) is achieved by the Minimum Mean Squared Error Estimation - Successive Interference Cancellation (MMSE-SIC) detector [25]. Here I(x;y) denotes the mutual information between the random variables x and y [26]. Therefore, for given channel parameters $\mathcal{P} = \{\{L_s\}_{s=1}^K, \{\theta_{s,i}, \phi_{s,i}, \tau_{s,i}, \nu_{s,i}, g_{s,i}\}_{s=1,i=1}^{K,L_s}\}$, the SE achieved by the proposed precoder in (17) with the optimal MMSE-SIC detector is given by (25). In (25), the factor $MN(1+\frac{\tau_{max}}{NT})$ is the total time-bandwidth product i.e., $M\Delta f(\tau_{max}+NT)$.

$$C_{s}(\mathcal{P}) \stackrel{\Delta}{=} \frac{I(\widehat{\mathbf{x}}_{s}; \mathbf{u}_{s})}{MN\left(1 + \frac{\tau_{max}}{NT}\right)} = \frac{1}{MN\left(1 + \frac{\tau_{max}}{NT}\right)} \times \log_{2} \left| \mathbf{I} + \frac{E_{T}}{\eta N_{o}} \mathbf{G}_{s,s} \mathbf{G}_{s,s}^{H} \left(\mathbf{I} + \frac{E_{T}}{\eta N_{o}} \sum_{\substack{s'=1, \ s' \neq s}}^{K} \mathbf{G}_{s,s'} \mathbf{G}_{s,s'}^{H} \right)^{-1} \right|.$$

$$(25)$$

The sum SE achieved by the proposed precoder is therefore given by

$$C(\mathcal{P}) \stackrel{\Delta}{=} \sum_{s=1}^{K} C_s(\mathcal{P}). \tag{26}$$

From (22) we know that the total transmitted energy is $E_T(\tau_{max}+NT)/(NT)$ and therefore the average total transmitted power is E_T/NT as the total duration of the OTFS frame is $(\tau_{max}+NT)$. At the receiver, the AWGN power is $M\Delta fN_o$ since N_o is the PSD of the AWGN and $M\Delta f$ is the total communication bandwidth. Subsequently, in this paper we denote the ratio of the average total transmitted power to the AWGN power at the receiver by

$$\rho \stackrel{\Delta}{=} \frac{E_T/(NT)}{M\Delta f N_o} = \frac{E_T}{MNN_o}$$
 (27)

which follows from the fact that $T\Delta f = 1$.

The complexity of the optimal MMSE-SIC detector is however $O(M^4\ N^4)$ and therefore, achieving the SE in (25) is challenging when M and/or N is large. In the next section, we therefore propose a low complexity detector which is shown to achieve a sum SE close to that of the optimal MMSE-SIC detector when the number of BS antennas (Q) is large.

V. LOW COMPLEXITY DETECTION OF RECEIVED MULTI-USER OTFS SIGNAL

In this section, we propose an alternate low complexity detector (LCD) where each information symbol in the DD domain is detected separately. In the following we propose the LCD for $u_{s,r}$ (the r-th element of \mathbf{u}_s). Let $\widehat{x}_{s,r}$ denote the r-th element of the DD domain vector $\widehat{\mathbf{x}}_s$ ($r=1,2,\ldots,MN$, $s=1,2,\ldots,K$) received at the s-th UT. From (23) it follows that

$$\widehat{x}_{s,r} = \sqrt{\frac{E_T}{\eta}} \, \gamma_{s,s,r,r} \, u_{s,r} \, + \, \widetilde{w}_{s,r} \,,$$

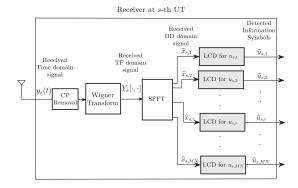


Fig. 3. Block diagram of the receiver at the s-th UT with the proposed LCD detector.

$$\tilde{w}_{s,r} \stackrel{\Delta}{=} \underbrace{\sqrt{\frac{E_T}{\eta}} \sum_{\substack{p=1\\p \neq r}}^{MN} \gamma_{s,s,r,p} u_{s,p}}_{\text{Inter-symbol Interference}} + \underbrace{\sqrt{\frac{E_T}{\eta}} \sum_{\substack{s'=1\\s' \neq s}}^{K} \sum_{p=1}^{MN} \gamma_{s,s',r,p} u_{s',p}}_{\text{AWGN}} + \underbrace{w_{s,r}}_{\text{AWGN}}$$
(28)

where $\gamma_{s,s',r,p}$ denotes the element of $\mathbf{G}_{s,s'}$ in its r-th row and p-th column. Here $w_{s,r}$ denotes the r-th element of \mathbf{w}_s . In (28), $\tilde{w}_{s,r}$ is the effective noise and interference and $\sqrt{\frac{E_T}{\eta}}\gamma_{s,s,r,r}\,u_{s,r}$ is the useful signal. The channel in (28) is effectively a singleinput single-output (SISO) channel with $u_{s,r}$ as input and $\hat{x}_{s,r}$ as output. Since $r = 1, 2, \dots, MN$, for each UT we therefore have MN sub-channels, one for each DDRE location (for example, from (13) and (28) it is clear that $u_{s,r}$ is transmitted and detected on the $(k = \lfloor (r-1)/M \rfloor, l = [r-1]_M)$ -th DDRE). At the encoder, different information codebooks are used in principle for generating information codewords for each such sub-channel of each UT. If the total communication time is limited to F OTFS frames and if $(c_{s,r,1}, c_{s,r,2}, \dots, c_{s,r,f}, \dots, c_{s,r,F})$ denotes the information codeword for the s-th UT to be transmitted on the r-th sub-channel, then the information symbol $c_{s,r,f}$ is transmitted in the f-th OTFS frame on the $(k = \lfloor (r-1)/M \rfloor, l = [r-1]_M)$ th DDRE (i.e., in the f-th OTFS frame, $u_{s,r} = c_{s,r,f}$). In the proposed LCD detector, the UT performs separate decoding for each SISO channel which greatly reduces the complexity when compared to MMSE-SIC. For example, if the received DD domain symbol in the f-th OTFS frame on the (k = |(r -1)/M, $l = [r-1]_M$ -th DDRE is denoted by $\widehat{x}_{s,r,f}$, then the codeword $(c_{s,r,1}, c_{s,r,2}, \dots, c_{s,r,f}, \dots, c_{s,r,F})$ is decoded from the received symbol vector $(\widehat{x}_{s,r,1},\widehat{x}_{s,r,2},\ldots,\widehat{x}_{s,r,F})$. In Fig. 3 we show the receiver at the s-th UT with the proposed LCD detector. Separate LCD detectors are shown for each of the MNsub-channels (see the shaded blocks in Fig. 3).

Due to separate symbol detection, the complexity of the LCD detector is O(MN) as there are MN information symbols in one OTFS frame. Since the complexity of the TF to DD domain conversion in (12) is $O(MN\log(MN))$, the overall complexity of LCD along with the TF to DD domain converter is only $O(MN\log(MN))$. Note that this complexity is independent of the number of channel paths and is smaller than the complexity

of the detector in [17] (which is at least $O(M^2 N^2)$). In the following we derive an expression for the achievable sum SE of the proposed LCD detector.

Theorem 1: For a given set of channel parameters $\mathcal{P}=\{\{L_s\}_{s=1}^K,\{\theta_{s,i},\phi_{s,i},\tau_{s,i},\nu_{s,i},g_{s,i}\}_{s=1,i=1}^{K,L_s}\}$, the SE achieved by the s-th UT with the proposed LCD detector is given by

$$R_s(\mathcal{P}) \stackrel{\Delta}{=} \frac{1}{MN\left(1 + \frac{\tau_{max}}{NT}\right)} \sum_{r=1}^{MN} I_{s,r}(\mathcal{P}),$$

$$I_{s,r}(\mathcal{P}) \stackrel{\Delta}{=} \log_2 \left(1 + \text{SINR}_{s,r}(\mathcal{P})\right),$$

$$SINR_{s,r}(\mathcal{P}) \stackrel{\Delta}{=}$$

$$\frac{\left|\gamma_{s,s,r,r}\right|^{2}}{\underbrace{\frac{\eta}{\rho MN}}_{\text{AWGN}} + \underbrace{\sum_{\substack{p=1 \\ p \neq r}}^{MN} \left|\gamma_{s,s,r,p}\right|^{2}}_{\text{Inter-symbol Interference (ISI)}} + \underbrace{\sum_{\substack{s'=1 \\ s' \neq s}}^{K} \sum_{p=1}^{MN} \left|\gamma_{s,s',r,p}\right|^{2}}_{\text{Multi-user Interference (MUI)}}.$$

Proof: For given channel parameters \mathcal{P} , the channel in (28) is a SISO channel with complex Gaussian information symbol $u_{s,r}$ and statistically independent effective noise and interference $\tilde{w}_{s,r}$. The statistical independence is due to i.i.d. information symbols $u_{s,p}$, $p=1,2,\ldots,MN$ and independent AWGN. The achievable rate expression in (29) then follows from the capacity of such SISO channels [25]. In (29), the factor $MN(1+\frac{T_{max}}{NT})$ is the total time-bandwidth product i.e., $M\Delta f(\tau_{max}+NT)$.

The sum SE achieved with the proposed LCD detector is therefore given by

$$R(\mathcal{P}) \stackrel{\Delta}{=} \sum_{s=1}^{K} R_s(\mathcal{P}). \tag{30}$$

Corollary 1: For fixed system and channel parameters i.e., fixed $(B_c, T_c, \Delta f, d/\lambda, \mathcal{P})$, as the URA size increases i.e., $(Q_h \to \infty, Q_v \to \infty)$ with constant ρQ , an approximation to $I_{s,r}$ is given by (31). From this approximation, it is clear that in the large (Q_h, Q_v) and small ρ regime, the achievable information rate of the proposed precoder with the LCD detector is limited only by AWGN, and becomes *independent* of intersymbol and multi-user interference.

$$I_{s,r} \overset{(a)}{\approx} \log_2 \left\lceil 1 + \left\{ \rho Q \left(\sum_{i=1}^{L_s} |g_{s,i}|^2 \right)^2 \middle/ \sum_{\tilde{s}=1}^K \sum_{i=1}^{L_{\tilde{s}}} \beta_{\tilde{s},i} \right\} \right\rceil,$$

Large (Q_h, Q_v) approximation with constant ρQ . (31)

Proof: Step (a) in (31) follows by substituting the large (Q_h,Q_v) approximation of $\gamma_{s,s',r,p}/Q$, $\gamma_{s,s,r,r}/Q$, $\gamma_{s,s,r,p}/Q$ from Appendices B, C, D and the expression for η from (17) into the expression for SINR_{s,r} in (29). From Appendices B and D we know that for large (Q_h,Q_v) (constant ρQ), $\gamma_{s,s',r,p}/Q \approx 0$ ($s \neq s'$) and for $p \neq r$, $\gamma_{s,s,r,p}/Q \approx 0$. Using this fact in the expression for SINR_{s,r} in (29), it is clear that in the large antenna and small ρ regime, the effective noise and interference power (i.e., denominator in the R.H.S. of the expression for SINR_{s,r} in (29)) is dominated by AWGN.

The following result shows that in the large (Q_h, Q_v) and small ρ regime, the proposed LCD detector is near-optimal.

Theorem 2: For fixed system and channel parameters i.e., fixed $(B_c, T_c, \Delta f, d/\lambda, \mathcal{P})$, as the URA size increases i.e.,

 $(Q_h \to \infty, Q_v \to \infty)$ with constant ρQ , the proposed LCD detector is near-optimal, i.e.,

$$R(\mathcal{P}) \approx C(\mathcal{P})$$
, Large (Q_h, Q_v) Approximation. (32)

Proof: Refer to Appendix E.

Discussion: From Corollary 1 and Theorem 2, the following conclusions can be made.

1) From Corollary 1 it is clear that with a large antenna array the achievable information rate with the proposed LCD detector depends on ρ only through the product ρQ , and therefore in the large (Q_h, Q_v) regime, for a desired achievable sum SE, the required ρ will decrease as 1/Qwith increasing (Q_h, Q_v) . This implies that the energy efficiency improves with increase in Q. This effect is the same as that observed in TF domain based OFDM massive MIMO systems with perfect channel state information (CSI) [18]. Also, just as in TF domain based massive MIMO systems, from Corollary 1 we also observe that even in OTFS based massive MIMO systems the effect of multi-user and inter-symbol interference vanishes with increasing number of BS antennas, i.e., in the large antenna and small ρ regime the sum SE is limited only by AWGN. From the proof of Corollary 1 it is clear that this happens due to the proposed precoder in (17), which results in combining of the channel matrices between the s-th UT and the BS (i.e., $\mathbf{H}_{q,s}, q = 1, 2, \dots, Q$) into the effective DD domain channel matrix $\mathbf{G}_{s,s} = \sum_{q=1}^{Q} \mathbf{H}_{q,s} \mathbf{H}_{q,s}^{H}$ (see (23) and (28)), whose off-diagonal entries are vanishingly smaller than its diagonal entries when Q is large (i.e., vanishing inter-symbol interference with increasing Q). Further, due to the proposed precoder, the channel matrices between the BS and the other UTs (i.e., $\mathbf{H}_{q,s'}, q = 1, 2, \dots, Q, s' \neq s$) combine with the channel matrices for the s-th UT resulting in the matrices $\mathbf{G}_{s,s'}=$ $\sum_{q=1}^{Q} \mathbf{H}_{q,s} \mathbf{H}_{q,s'}^{H}$ which cause multi-user interference (see (23) and (28)), but whose entries are vanishingly small (compared to the diagonal entries of $G_{s,s}$) with increasing Q. From Theorem 2 it is further clear that in the large antenna and small ρ regime, the proposed LCD detector is near-optimal i.e., $R(\mathcal{P}) \approx C(\mathcal{P})$.

VI. NUMERICAL SIMULATIONS

For numerical simulations, we consider a single circular cell of radius 5 Km with a $Q=Q_hQ_v$ antenna BS at its centre serving K single antenna UTs in the downlink. The UTs are uniformly distributed in the cell except in a circular region of radius 35 m around the BS. We consider the Rural Macro Non Line-of-Sight (RMa-NLOS) scenario which is expected to be deployed for wide area coverage (e.g., supporting high speed vehicles) [27]. The path-loss model, the power delay profile (i.e., number of paths, path delays and their relative power gains) and the angles of departure are described in Section 7.4.1 and Table 7.5 - 6 (Part-2) in [27]. The Doppler shift for each path is modelled as $\nu_{s,i} = \nu_{max} \cos(\alpha_{s,i})$ where $\alpha_{s,i}$ are distributed uniformly in $[0, 2\pi)$. Further, $\alpha_{s,i}$ are statistically independent

 $^{^5}$ As a reference, we consider the path-loss to a cell-edge UT to be unity and therefore the variable ρ denotes the average received signal-to-noise ratio (in the time-domain) at a cell-edge UT.

 $^{^6 \}text{As the cell-size}$ (5 Km radius) is not small, we consider a mean delay spread of $0.37 \mu s.$

TABLE I
System Parameters

Parameter	Value
Carrier Frequency (f_c)	4.8 GHz
Sub-carrier Spacing (Δf)	15 KHz
M, N	M = 330, N = 4
Bandwidth (B_c)	$B_c = M\Delta f = 4.95 \text{ MHz}$
OTFS Frame Duration (T_c)	$T_c = N/\Delta f = 0.266 \text{ ms}$

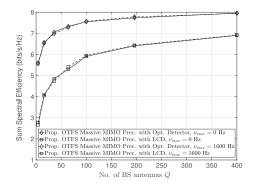


Fig. 4. Sum SE (bits/s/Hz) versus number of BS antennas Q (constant $\rho \, Q = 0.1$).

for different $s=1,2,\ldots,K$ and $i=1,2,\ldots,L_s$. The spacing between adjacent antenna elements in the URA is taken to be half of the carrier wavelength. The maximum possible channel path delay is taken to be $\tau_{max}=4.7\mu s$, which is the CP size in 4G-LTE systems. The system parameters $(B_c,\Delta f,T_c,M,N,f_c)$ are tabulated in Table-I.

In Fig. 4, we plot the sum SE achieved by the proposed OTFS based precoder with two different detectors, i.e., i) optimal MMSE-SIC detector, and ii) proposed LCD detector. The SEs are plotted as a function of increasing URA size Q (with $Q_h = Q_v$) and a constant $\rho Q = 0.1$. The plotted SEs are averaged over the statistics of the channel parameters $\mathcal{P} = \{\{L_s\}_{s=1}^K, \{\theta_{s,i}, \phi_{s,i}, \tau_{s,i}, \nu_{s,i}, g_{s,i}\}_{s=1,i=1}^{K,L_s}\}$. Therefore, the plotted SE is $\mathbb{E}[C(\mathcal{P})]$ and $\mathbb{E}[R(\mathcal{P})]$ respectively for the optimal detector and the proposed LCD detector (see (26) and (30)). There are K = 4 UTs and we consider two scenarios, i) where the maximum Doppler shift for each UT is $\nu_{max} = 1600$ Hz which corresponds to a mobile speed of 360 Km/hr at a carrier frequency of $f_c = 4.8$ GHz, and ii) where the UTs are stationary (i.e., $\nu_{max}=0$). The other system parameters are as in Table-I. From Fig. 4 it is clear that the gap between the SE achieved by the LCD detector and that achieved by the optimal detector diminishes with increasing number of BS antennas. This supports our analysis in Theorem 2. It is also observed that for both the detectors, the SE at a high mobile speed of 360 Km/hr (i.e., $\nu_{max} = 1600 \text{ Hz}$) is almost same as the SE at zero mobile speed, i.e., the SE is almost *invariant* to channel induced Doppler shift.

In Fig. 5, we plot the average sum SE achieved by the proposed downlink precoder with the proposed LCD detector (i.e., $\mathbb{E}[R(\mathcal{P})]$), for a OTFS multi-user massive MIMO downlink system as a function of increasing maximum Doppler shift ν_{max} . The BS has a URA of size $Q_h = Q_v = 14$, i.e., Q = 196 antennas, $\rho Q = 0.1$ and K = 4 UTs. The other system parameters are as in Table-I. In Fig. 5, we also plot the SE achieved by the proposed downlink precoder with the optimal detector in the

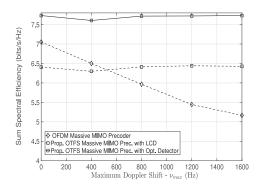


Fig. 5. Sum SE (bits/s/Hz) versus maximum Doppler shift ν_{max} (Hz).

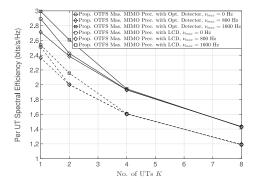


Fig. 6. Per UT SE (bits/s/Hz) versus number of UTs K.

DD domain (i.e., $\mathbb{E}[C(\mathcal{P})]$), and the SE achieved by an OFDM multi-user massive MIMO downlink system (with Maximum Ratio Transmission precoding in the TF domain [18]). The sub-carrier spacing for the OFDM massive MIMO system is $\Delta f = 15$ KHz. From the figure it is clear that the SE achieved by OFDM massive MIMO degrades significantly at high mobile speed whereas the SE achieved by the proposed precoder (with either the LCD detector or the optimal detector) does not degrade. At high mobile speed, the proposed DD domain based downlink precoder with the LCD detector achieves significantly better SE when compared to that achieved by an OFDM massive MIMO system.

In Table-II we list the sum SE achieved by the proposed OTFS based downlink precoder with the LCD detector and that achieved by the OFDM massive MIMO system as a function of varying ρ when the BS has Q=196 BS antennas ($Q_h=Q_v=14$) and there are K=4 UTs. From the table, it is observed that for all considered values of ρ , at high Doppler spread the sum SE achieved by OTFS massive MIMO is significantly greater than that achieved by OFDM massive MIMO. Also, for all considered values of ρ , the sum SE achieved by the OTFS massive MIMO system is almost invariant of the Doppler spread.

In Fig. 6, we plot the per UT SE achieved by the proposed downlink precoder with both the LCD and the optimal detector (i.e., $\mathbb{E}[R(\mathcal{P})]/K$ and $\mathbb{E}[C(\mathcal{P})]/K$ respectively) as a function of increasing number of UTs K. The BS has a URA of size $Q_h = Q_v = 14$, i.e., Q = 196 antennas and $\rho Q = 0.1$. From the figure we observe that the gap between the per UT SE achieved by the proposed LCD detector and that by the optimal detector is around 0.4 bits/s/Hz with K = 2 UTs, but decreases to 0.2 bits/s/Hz when the number of UTs is increased to K = 8.

In Fig. 7, we plot the variation in the sum SE achieved by the proposed precoder as a function of varying power delay profile,

ſ		$\rho Q =$	-19 dB	$\rho Q = -16 \text{ dB}$		$\rho Q = -13 \text{ dB}$		$\rho Q = -10 \text{ dB}$		$\rho Q = -7 \text{ dB}$	
Ì		OTFS	OFDM	OTFS	OFDM	OTFS	OFDM	OTFS	OFDM	OTFS	OFDM
Ì	$\nu_{max} = 0 \text{ Hz}$	4.4	4.6	5.0	5.4	5.7	6.2	6.4	7.1	7.1	8.1
Ì	$\nu_{max} = 400 \text{ Hz}$	4.4	4.2	5.0	4.9	5.6	5.6	6.3	6.4	7.0	7.2
Ì	$\nu_{max} = 800 \text{ Hz}$	4.4	3.9	5.0	4.5	5.7	5.2	6.4	5.9	7.1	6.6
Ì	$\nu_{max} = 1200 \text{ Hz}$	4.5	3.7	5.0	4.2	5.7	4.8	6.4	5.5	7.1	6.2
Ì	$\nu_{max} = 1600 \text{ Hz}$	4.5	3.5	5.0	4.0	5.7	4.6	6.4	5.2	7.1	5.9

TABLE II SUM SE (bits/s/Hz) VS. $(\nu_{max}, \rho Q), Q_h = Q_v =$ 14, $Q = Q_h Q_v =$ 196, K = 4 UTS

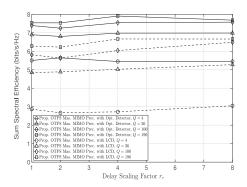


Fig. 7. Sum SE (bits/s/Hz) vs. delay scaling factor r_{τ} .

but fixed number of UTs K=4, fixed $\rho Q=0.1$ and fixed $\nu_{max}=1600$ Hz. In the RMa-NLOS channel model [27], the random channel path delays are modelled as $\tau=-r_{\tau}\mu_{\tau}\log(X)$ where X is uniformly distributed in the interval $[0\,,\,1]$. The power gain of a path having delay τ is proportional to $e^{-\tau\frac{(r_{\tau}-1)}{r_{\tau}\mu_{\tau}}}$. Here μ_{τ} is the mean delay spread and r_{τ} is the delay scaling factor which can be used to vary the power profile of the channel paths. A value of $r_{\tau}=1$ models a flat power profile where all channel paths have the same power irrespective of their delay. With increasing r_{τ} , the power profile becomes steeper, i.e., the power of channel paths decreases more rapidly with increasing path delay. From Fig. 7 it is clear that the SE achieved by the proposed OTFS massive MIMO precoder is almost invariant of the power profile and does not degrade when there are a large number of equal power paths (i.e., when r_{τ} is close to 1).

A. Coded Error Rate Performance Comparison Between OTFS and OFDM Massive MIMO Systems With Imperfect CSI

In this section, we present the comparison between the error rate performance of the proposed OTFS precoder (with the LCD detector) and the OFDM massive MIMO precoder, for the imperfect channel state information (CSI) scenario. In both the proposed OTFS system and the OFDM based system, we perform uplink channel estimation and the estimated uplink channel is used for downlink precoding. This strategy is used since we consider a TDD system where the uplink and downlink channels are reciprocal.

For the OTFS based system, since $T=1/\Delta f=66.66\mu s$, each OTFS frame is $(\tau_{max}+NT)=4.7+4\times66.66=271.37\,\mu s$ in duration. As shown in Fig. 8, downlink communication consists of a sequence of 35 consecutive OTFS frame of total duration $35\times271.37\mu s=9.5$ ms. We consider a rate-1/3 Turbo code (see 3GPP Technical Standard (TS) 36.212: Multiplexing and Channel Coding) and 4-QAM modulation of coded

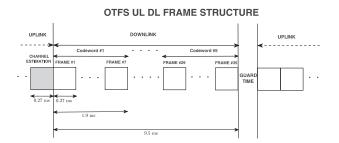


Fig. 8. OTFS Uplink (UL) and Downlink (DL) communication.

bits to information symbols. Each codeword has 6144 information bits and therefore consists of $3 \times (6144 + 4)/2 = 9222$ 4-QAM symbols. Since each OTFS frame can carry $M \times N = 330 \times 4 = 1320$ symbols, a codeword spans $\lceil 9222/1320 \rceil = 7$ OTFS frames having duration $7 \times 271.37 \, \mu s = 1.9$ ms. Therefore, five codewords can be transmitted in 35 OTFS frames over a duration of 9.5 ms. As discussed earlier in Section II, the channel path delays, Doppler shifts and channel path gains are assumed to be fixed for a few tens of ms, and therefore in our simulations we consider them to be constant for one OTFS uplink phase followed by a downlink phase i.e., $2 \times 9.5 = 19$ ms (we assume alternate uplink and downlink communication phases, with each phase of 9.5 ms duration). Uplink channel estimation is performed in the last OTFS frame of each uplink communication phase (see Fig. 8).

Although the OTFS channel matrices $(MN \times MN)$ are large for large M and/or N, they depend on the path parameters (i.e., path gains, path delays and Doppler shifts) of only a small number of paths $(L_s \ll MN, s=1,2,\ldots,K,$ see also (15)). Therefore, we consider low-complexity estimation of these parameters, which has been described in detail in Appendix F. As discussed above, we consider the use of only one OTFS frame for transmission of uplink pilots. Through simulations (discussed later in this section) we show that the coded error rate performance with the proposed channel estimation is almost the same as that with perfect channel knowledge. As the same channel estimate is used for both uplink and downlink communication and only one pilot OTFS frame is sufficient, the channel estimation overhead is $\frac{100}{(2\times35)}=1.43$ percent only.

For the OFDM based massive MIMO system also, we consider alternate uplink and downlink communication phases of equal duration. Uplink pilots transmitted by the UTs are used by the BS to acquire channel estimates. As shown in Fig. 9, at the end of the uplink communication phase an OFDM symbol is dedicated for the transmission of uplink pilot for each UT. Therefore with K=4 UTs, four OFDM symbols are dedicated for uplink channel estimation. In each OFDM pilot symbol, pilots are transmitted on each sub-carrier and separate channel estimation for each sub-carrier is performed on all the Q receive

OFDM UL DL FRAME: OPTION I

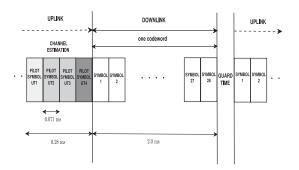


Fig. 9. OFDM UL and DL frames with one codeword transmitted in one DL frame.

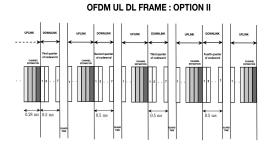


Fig. 10. OFDM UL and DL frames with one codeword spanning four DL frames.

antennas at the BS. In OFDM, the TF domain channel changes due to the Doppler shift induced by each multi-path and therefore we consider two different UL-DL frame options. In option-I shown in Fig. 9, one codeword (same as that described earlier for the OTFS based system) consisting of 9222 4-QAM symbols is transmitted in the downlink in $\lceil 9222/330 \rceil = 28$ OFDM symbols, which spans a duration of $28 \times 71.36~\mu s = 2.0$ ms (as each OFDM symbol is $1/\Delta f + 4.7\mu s = 71.36~\mu s$). The channel estimation overhead with option-I ($K=4~\rm UTs$) is therefore $\frac{K}{(2 \times 28)} \times 100 = 7.14$ percent.

In option-II as shown in Fig. 10, the pilots are transmitted more frequently to support higher mobility than that supported by option-I. Specifically, one codeword is transmitted in four downlink communication phases. As channel estimation is performed at the end of each uplink phase, the channel estimation overhead with option-II is therefore $\frac{K}{2\times 7} \times 100 = 28.6$ percent. Also, the total time duration between the first channel estimation just before the start of transmission of a codeword and the end of transmission of that codeword is roughly $32 \times 71.36 \, \mu s = 2.28$ ms and $53 \times 71.36 \, \mu s = 3.78$ ms for option-I and option-II respectively. For these durations, the underlying channel path gains $h_{q,s,i}$, path delays $\tau_{s,i}$ and Doppler shifts $\nu_{s,i}$ do not change, but the TF domain channel changes due to the Doppler shifts of the channel paths.

In Fig. 11, we compare the Frame Error Rate (FER) (i.e., codeword error rate) performance of the proposed OTFS massive MIMO precoder (with the LCD detector) and OFDM massive MIMO as a function of increasing ρ for a fixed $Q_h = Q_v = 14$ and K = 4 UTs. We consider the imperfect CSI scenario where the received pilot signal to noise ratio at each BS antenna is 26 dB for both OTFS and OFDM systems. We note that the FER performance of OFDM massive MIMO with option-I and

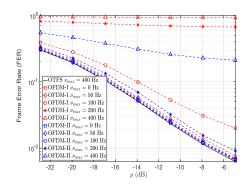


Fig. 11. FER vs. ρ for OTFS and OFDM massive MIMO.

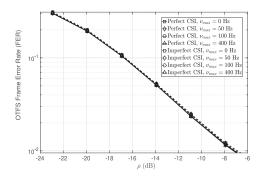


Fig. 12. FER vs. ρ for OTFS massive MIMO.

option-II UL-DL frames (denoted in the figure as OFDM-I and OFDM-II respectively), degrades with increase in Doppler spread. Even with frequent transmission of uplink pilots (i.e., OFDM-II with a pilot overhead of 28.6 percent), the FER performance at $\nu_{max}=400$ Hz is poor when compared to that of OTFS massive MIMO with a pilot overhead of *only* 1.43 percent. Therefore, the proposed OTFS massive MIMO precoder achieves significantly *better* error rate performance than OFDM massive MIMO, with much *lower* pilot overhead.

In Fig. 12, we plot the FER for OTFS massive MIMO with the proposed precoder (and the LCD detector) as a function of increasing ρ for a fixed number of BS antennas ($Q_h = Q_v = 14$) and K = 4 UTs. We consider both the perfect and imperfect CSI scenarios. For the imperfect CSI scenario, the received pilot signal to noise ratio at each BS antenna is $\rho_p = 26$ dB (see Appendix F). With increasing maximum Doppler shift ν_{max} , multi-user interference (MUI) and inter-symbol interference (ISI) could increase. However, due to the proposed precoder in (17), MUI and ISI become vanishingly small in comparison to AWGN, when the number of BS antennas (Q_h, Q_v) is sufficiently large (see proof of Corollary 1 and the Discussion segment after (32)). In fact, from (31) it is clear that the large (Q_h, Q_v) approximation of the SE achieved by a UT is independent of the multi-path Doppler shift. Hence, for the perfect CSI scenario, with large (Q_h, Q_v) the FER performance is also expected to be almost invariant of the multi-path Doppler shift. This is in fact observed in Fig. 12.7 From Fig. 12 we also observe that the FER performance for the perfect and imperfect CSI

 $^{^{7}}$ One more reason for the same FER performance for all ν_{max} considered in Fig. 12 is that multi-path Doppler diversity is not obtained as the maximum Doppler shift ν_{max} is significantly less than the Doppler domain resolution [28]. As the main objective of this paper is to propose a low complexity multi-user precoder and low-complexity decoder for OTFS massive MIMO systems, we do not consider achieving Doppler diversity here, although it is an interesting future work.

scenarios are the same, which shows the effectiveness of the OTFS channel estimation considered in Appendix F.⁸

VII. CONCLUSION

In this paper, we have proposed a low complexity OTFS multiuser massive MIMO precoder where multi-user precoding is performed in the DD domain. As the optimal MMSE-SIC based detector at each UT has prohibitive complexity when (M, N)is large, we also propose a low complexity LCD detector for detection of information symbols at each UT. Through analysis we show that with increasing number of BS antennas the sum SE performance of the proposed LCD detector converges to that achieved by the optimal detector. Through simulations we also show that the proposed OTFS multi-user massive MIMO precoder achieves significantly better SE than a OFDM multiuser massive MIMO precoder in high mobility scenarios where the Doppler shift of the channel paths is high. Simulations of the coded error rate performance reveals that OTFS massive MIMO achieves significantly better FER than OFDM massive MIMO with much smaller pilot overhead.

APPENDIX A DERIVATION OF (14) AND (15)

Substituting the expression for $x_a(t)$ from (10) into the R.H.S. of (5), we get an expression for $y_s(t)$ in terms of the DD domain signals $x_q[k, l], q = 1, 2, \dots, Q$. Using this expression of $y_s(t)$ into the R.H.S. of (11) we get an expression for $Y_s[n, m]$ which when substituted in the R.H.S. of (12) gives an expression for $\widehat{x}_s[k,l]$ in terms of $x_a[k,l]$, i.e.

$$\widehat{x}_s[k,l] \stackrel{(a)}{=} \frac{1}{MN} \sum_{q=1}^{Q} \sum_{k'=0}^{N-1} \sum_{l'=0}^{M-1} x_q[k',l'] \, \widetilde{h}_{q,s,k,l}[k',l']$$

$$+ w_s[k,l]$$

$$\tilde{h}_{q,s,k,l}[k',l'] \stackrel{\Delta}{=} \frac{1}{MN} \left(h_{q,s,k,l}^{\text{ici}}[k',l'] + e^{-j2\pi \frac{k'}{N}} h_{q,s,k,l}^{\text{isi}}[k',l'] \right)$$
(33)

where step (a) follows from equations (53) and (60) in Appendix C of [5] and the expressions for $h_{q,s,k,l}^{\rm ici}[k',l']$ and $h_{q,s,k,l}^{\rm isi}[k',l']$ follow from equations (56) and (61) respectively in [5] (see (34), at the bottom of this page).

Note that in (34), $l_{\tau_{s,i}} \stackrel{\triangle}{=} \tau_{s,i} M \Delta f$ is an integer. In the R.H.S. of equation (61) in [5], the expression for the ISI term consists of

a summation over n = 1 to n = N - 1 whereas the expression for the ICI term in equation (56) of [5] consists of a summation over n=0 to n=N-1. This is due to the fact that in [5], instead of the CP, zero prefix of duration τ_{max} is used to avoid interference between consecutive OTFS frames in the time-domain. Due to this, in [5], the sum over n in the ISI term is -1/N less than the sum over n in the ICI term. This difference is significant when N is not large and can reduce the energy of the effective DD domain channel gains $\tilde{h}_{q,s,k,l}[k',l']$. Therefore, in this paper we have considered a CP of length τ_{max} , due to which the summation over n will be from n = 0 to n = N - 1in both the ICI and the ISI terms (see (34)).

In (33), the received additive noise sample on the (k, l)-th DDRE is given by

$$w_s[k, l] \stackrel{\Delta}{=} \frac{1}{\sqrt{MN}} \sum_{n=0}^{N-1} \sum_{m=0}^{M-1} W_s[n, m] e^{-j2\pi \left(\frac{nk}{N} - \frac{ml}{M}\right)}$$

$$k = 0, 1, \dots, N - 1, l = 0, 1, \dots, M - 1$$
 (35)

where $W_s[n,m]$ is the received noise sample in the (n,m)-th TFRE. Further, from (5) and (11), $W_s[n, m]$ is given by

$$W_s[n, m] = \int g_{rx}^*(t - nT)\tilde{w}_s(t) e^{-j2\pi m\Delta f(t - nT)} dt.$$
 (36)

Since $\tilde{w}_s(t)$ is AWGN with power spectral density N_0 , from (35) and (36) it follows that

$$w_s[k,l] \sim \text{i.i.d. } \mathcal{CN}(0,N_0).$$
 (37)

 $w_s[k,l] \sim \text{i.i.d.}\,\mathcal{CN}(0,N_0). \tag{37}$ Let $\mathbf{H}_{q,s} \in \mathbb{C}^{MN \times MN}$ denote a matrix whose element in its (kM+l+1)-th row and (k'M+l'+1)-th column is $h_{q,s,k,l}[k',l']$ (see (33)). Then, arranging $\hat{x}_s[k,l], x_q[k,l]$ and $w_s[k, l]$ respectively into the vectors $\hat{\mathbf{x}}_s, \mathbf{x}_q$ and \mathbf{w}_s (see (13)) and using (33), we get (14). Further, from (14) and the expressions for $h_{q,s,k,l}^{\rm ici}[k',l']$ and $h_{q,s,k,l}^{\rm isi}[k',l']$ in (34) it follows that

$$\tilde{h}_{q,s,k,l}[k',l'] \stackrel{\Delta}{=} \sum_{i=1}^{L_s} h_{q,s,i} \, a_{s,i,k,l}[k',l']$$
 (38)

where $a_{s,i,k,l}[k',l']$ is given by (39), as shown at the bottom of the next page.

In (39), the discrete impulse sequence $\delta[p](p \in \mathbb{Z})$ is one when p = 0 and is zero otherwise. In the first equation in (39), $a_{s,i,k,l}[k',l']$ is a sum of two terms, the first term in the first line and the second term below it. Since the delays are integer multiple of $1/(M\Delta f),\, l_{\tau_{s,i}}=M\Delta f \tau_{s,i}$ is an integer. Therefore, in the R.H.S. of the first equation in (39), we observe that each term is non-zero only when the summation variable p equals l' (see the last inner summation over m' which equals $\delta[[p-l']_M]$). Also, the inner summation over m is non-zero only when $p = [l - l_{\tau_{s,i}}]_{\scriptscriptstyle M}$. From these two facts it follows that $a_{s,i,k,l}[k',l']$ is non-zero only when $[l'+l_{ au_{s,i}}-l]_{\scriptscriptstyle M}$ is zero, i.e., $l = [l' + l_{\tau_{s,i}}]_M$. In the first line of the first equation in (39), the summation over p is from p = 0 to $p = M - 1 - l_{\tau_s}$, and since

$$\frac{h_{q,s,k,l}^{\text{ici}}[k',l'] = \sum_{i=1}^{L_s} \frac{h_{q,s,i}}{M} \left\{ \left(\sum_{n=0}^{N-1} e^{j2\pi n \left(\frac{\nu_{s,i}}{\Delta f} - \frac{(k-k')}{N} \right)} \right) \left[\sum_{p=0}^{M-1-l_{\tau_{s,i}}} e^{j2\pi \frac{p}{M} \left(\frac{\nu_{s,i}}{\Delta f} \right)} \sum_{m=0}^{M-1} e^{-j2\pi \left(p + l_{\tau_{s,i}} - l \right) \left(\frac{m}{M} \right)} \sum_{m'=0}^{M-1} e^{j2\pi (p-l') \frac{m'}{M}} \right] \right\} \\
h_{q,s,k,l}^{\text{isi}}[k',l'] = \sum_{i=1}^{L_s} \frac{h_{q,s,i}}{M} \left\{ \left(\sum_{n=0}^{N-1} e^{j2\pi n \left(\frac{\nu_{s,i}}{\Delta f} - \frac{(k-k')}{N} \right)} \right) \left[\sum_{p=M-l_{\tau_{s,i}}}^{M-1} e^{j2\pi \left(\frac{p-M}{M} \right) \frac{\nu_{s,i}}{\Delta f}} \sum_{m=0}^{M-1} e^{-j2\pi \left(p + l_{\tau_{s,i}} - l \right) \left(\frac{m}{M} \right)} \sum_{m'=0}^{M-1} e^{j2\pi (p-l') \frac{m'}{M}} \right] \right\}$$
(34)

⁸For high maximum Doppler shift (ν_{max}) also, the FER performance in the imperfect CSI scenario is the same as that in the perfect CSI scenario. This is because, the OTFS channel estimation in Appendix F estimates the exact Doppler shift of each path (i.e., for the *i*-th path it estimates ν_i completely and not just its integer part $\lfloor \frac{\nu_i}{\Delta f/N} \rfloor \frac{\Delta f}{N}$), and that the Doppler estimate in Appendix F is accurate at high received pilot signal to noise ratio ρ_p .

this term can only be non-zero if p=l', it follows that this term contributes to $a_{s,i,k,l}[k',l']$ if and only if $l'\in[0\,,\,M-1-l_{\tau_{s,i}}]$. Similarly, the term in the second line of (39) contributes to $a_{s,i,k,l}[k',l']$ if and only if $l'\in[M-l_{\tau_{s,i}}\,,\,M-1]$. The second equation in (39) then follows from these observations.

equation in (39) then follows from these observations. Let $\mathbf{A}_{s,i} \in \mathbb{C}^{MN \times MN}$ denote the matrix whose element in its (kM+l+1)-th row and (k'M+l'+1)-th column is $a_{s,i,k,l}[k',l']$. Since $\tilde{h}_{q,s,k,l}[k',l']$ denotes the element of $\mathbf{H}_{q,s}$ in its (kM+l+1)-th row and (k'M+l'+1)-th column, (15) follows from (38). Let $\mathbf{a}_{s,i,r} \in \mathbb{C}^{MN \times 1}$ denote the r-th column of $\mathbf{A}_{s,i}^H$, $r=1,2,\ldots,MN$. For any $s=1,2,\ldots,K$, $i=1,2,\ldots,L_s$ and $r=1,2,\ldots,MN$, the second equation in (39) gives the expression for the elements in the r-th row of $\mathbf{A}_{s,i}$. Therefore, for the r=(kM+l+1)-th row of $\mathbf{A}_{s,i}$ i.e., $\mathbf{a}_{s,i,r}^H$, we have $k=\lfloor r/M \rfloor$ and $l=[r]_M$. With this (k,l) pair (which corresponds to the r-th row of $\mathbf{A}_{s,i}$), from (39) we have

$$\|\mathbf{a}_{s,i,r}\|^{2} = \frac{1}{N^{2}} \sum_{k'=0}^{N-1} \left| \sum_{n=0}^{N-1} e^{j2\pi n \left(\frac{\nu_{s,i}}{\Delta f} - \frac{(k-k')}{N}\right)} \right|^{2}$$

$$= \frac{1}{N^{2}} \sum_{k'=0}^{N-1} \sum_{n_{1}=0}^{N-1} \sum_{n_{2}=0}^{N-1} e^{j2\pi (n_{1} - n_{2}) \left(\frac{\nu_{s,i}}{\Delta f} - \frac{(k-k')}{N}\right)}$$

$$= \frac{1}{N^{2}} \sum_{n_{1}=0}^{N-1} \sum_{n_{2}=0}^{N-1} e^{j2\pi (n_{1} - n_{2}) \left(\frac{\nu_{s,i}}{\Delta f} - \frac{k}{N}\right)}$$

$$\underbrace{\left[\sum_{k'=0}^{N-1} e^{j2\pi (n_{1} - n_{2}) \frac{k'}{N}}\right]}_{=N \delta[n_{1} - n_{2}]}$$

$$= 1. \tag{40}$$

Similarly, from the second equation in (39) it also follows that for any $r_1, r_2 = 1, 2, ..., MN$ and $r_1 \neq r_2$

$$\mathbf{a}_{s,i,r_1}^H \mathbf{a}_{s,i,r_2} = 0.$$
 (41)

From (40) and (41) we then have

$$\mathbf{A}_{s,i}\mathbf{A}_{s,i}^{H} = \mathbf{I}, \ \mathbf{A}_{s,i}^{H}\mathbf{A}_{s,i} = \mathbf{I}. \tag{42}$$

$\begin{array}{c} \text{Appendix B} \\ \text{Expression for } \gamma_{s,s',r,p}/Q \quad (s \neq s') \end{array}$

Let $\mathbf{a}_{s,i,r} \in \mathbb{C}^{MN \times 1}$ denote the r-th column of $\mathbf{A}_{s,i}^H$. Then, from (24) we have

$$\frac{\gamma_{s,s',r,p}}{Q} = \sum_{q=1}^{Q} \sum_{i=1}^{L_s} \sum_{k=1}^{L_{s'}} (h_{q,s,i} h_{q,s',k}^*/Q) \mathbf{a}_{s,i,r}^H \mathbf{a}_{s',k,p}$$

$$= \sum_{i=1}^{L_s} \sum_{k=1}^{L_{s'}} \left(\sum_{q=1}^{Q} h_{q,s,i} h_{q,s',k}^*/Q \right) \mathbf{a}_{s,i,r}^H \mathbf{a}_{s',k,p}. \tag{43}$$

From (2) it follows that

$$\left(\sum_{q=1}^{Q} h_{q,s,i} h_{q,s',k}^{*} / Q\right) \\
= \frac{g_{s,i} g_{s',k}^{*}}{Q_{h} Q_{v}} \sum_{q=1}^{Q} e^{j2\pi \frac{d}{\lambda} \left([q-1]_{Q_{h}} b_{s,s',i,k} + \left\lfloor \frac{q-1}{Q_{h}} \right\rfloor c_{s,s',i,k}\right)} \\
= \frac{g_{s,i} g_{s',k}^{*}}{Q_{h} Q_{v}} \left[\sum_{q_{h}=0}^{Q_{h}-1} e^{j2\pi \frac{d}{\lambda} q_{h} b_{s,s',i,k}} \right] \left[\sum_{q_{v}=0}^{Q_{v}-1} e^{j2\pi \frac{d}{\lambda} q_{v} c_{s,s',i,k}} \right] \\
= \left[g_{s,i} g_{s',k}^{*} e^{j\pi \frac{d}{\lambda} \left((Q_{h}-1)b_{s,s',i,k} + (Q_{v}-1)c_{s,s',i,k}\right)} \right] \\
\frac{\sin(\frac{d}{\lambda} b_{s,s',i,k} Q_{h})}{\sin(\frac{d}{\lambda} b_{s,s',i,k})} \frac{\sin(\frac{d}{\lambda} c_{s,s',i,k} Q_{v})}{\sin(\frac{d}{\lambda} c_{s,s',i,k})} \\
b_{s,s',i,k} \stackrel{\triangle}{=} \sin(\phi_{s,i}) \sin(\theta_{s,i}) - \sin(\phi_{s',k}) \sin(\theta_{s',k}) , \\
c_{s,s',i,k} \stackrel{\triangle}{=} \cos(\theta_{s,i}) - \cos(\theta_{s',k}). \tag{44}$$

Using (44) in (43) we get

$$\frac{\gamma_{s,s',r,p}}{Q} = \sum_{i=1}^{L_s} \sum_{k=1}^{L_{s'}} \mathbf{a}_{s,i,r}^H \, \mathbf{a}_{s',k,p} e^{j\pi \frac{d}{\lambda} \left((Q_h - 1)b_{s,s',i,k} + (Q_v - 1)c_{s,s',i,k} \right)}$$

 $a_{s,i,k,l[k',l']}$

$$\frac{=\delta\left[[p+l_{\tau_{s,i}}-l]_{M}\right]}{\left\{\frac{1}{N}\sum_{n=0}^{N-1}e^{j2\pi n\left(\frac{\nu_{s,i}}{\Delta f}-\frac{(k-k')}{N}\right)}\right)\left[\sum_{p=0}^{M-1-l_{\tau_{s,i}}}e^{j2\pi\frac{p}{M}\left(\frac{\nu_{s,i}}{\Delta f}\right)}\left\{\frac{1}{M}\sum_{m=0}^{M-1}e^{-j2\pi\left(p+l_{\tau_{s,i}}-l\right)\left(\frac{m}{M}\right)}\right\}\left\{\frac{1}{M}\sum_{m'=0}^{M-1}e^{j2\pi\left(p-l'\right)\frac{m'}{M}}\right\}\right]} + \left(\frac{1}{N}\sum_{n=0}^{N-1}e^{j2\pi n\left(\frac{\nu_{s,i}}{\Delta f}-\frac{(k-k')}{N}\right)}\right)\left[\sum_{p=M-l_{\tau_{s,i}}}^{M-1}e^{j2\pi\left(\frac{p-M}{M}\right)\frac{\nu_{s,i}}{\Delta f}}\left\{\frac{1}{M}\sum_{m=0}^{M-1}e^{-j2\pi\left(p+l_{\tau_{s,i}}-l\right)\left(\frac{m}{M}\right)}\right\}\left\{\frac{1}{M}\sum_{m'=0}^{M-1}e^{j2\pi\left(p-l'\right)\frac{m'}{M}}\right\}\right]}{=\delta\left[[p-l']_{M}\right]} = \left\{0, \qquad \qquad l \neq [l'+l_{\tau_{s,i}}]_{M} \\ \left[\frac{1}{N}\left[\sum_{n=0}^{N-1}e^{j2\pi n\left(\frac{\nu_{s,i}}{\Delta f}-\frac{(k-k')}{N}\right)}\right]e^{j2\pi\frac{l'}{M}\frac{\nu_{s,i}}{\Delta f}}, \qquad l = [l'+l_{\tau_{s,i}}]_{M}, l' \in [0, M-1-l_{\tau_{s,i}}]}\\ \left[\sum_{n=0}^{N-1}e^{j2\pi n\left(\frac{\nu_{s,i}}{\Delta f}-\frac{(k-k')}{N}\right)}\right]e^{j2\pi\left(\frac{l'}{M}\frac{\nu_{s,i}}{\Delta f}-\frac{\nu_{s,i}}{N}\right)}, \quad l = [l'+l_{\tau_{s,i}}]_{M}, l' \in [M-l_{\tau_{s,i}}, M-1]}$$

$$k' = 0, 1, \dots, N-1, \quad k = 0, 1, \dots, N-1, \quad l' = 0, 1, \dots, M-1, \quad l = 0, 1, \dots, M-1$$

$$(39)$$

$$g_{s,i} g_{s',k}^* \frac{\operatorname{sinc}(\frac{d}{\lambda} b_{s,s',i,k} Q_h)}{\operatorname{sinc}(\frac{d}{\lambda} b_{s,s',i,k})} \frac{\operatorname{sinc}(\frac{d}{\lambda} c_{s,s',i,k} Q_v)}{\operatorname{sinc}(\frac{d}{\lambda} c_{s,s',i,k})}.$$
(45)

Since the azimuthal and zenith angles for any two UTs are not the same, for any $s \neq s'$, at least one among $b_{s,s',i,k}$ and $c_{s,s',i,k}$ is not zero. Hence, for all $s \neq s'$, $\frac{\sin(\frac{d}{\lambda}b_{s,s',i,k}Q_h)}{\sin(\frac{d}{\lambda}b_{s,s',i,k})} \frac{\sin(\frac{d}{\lambda}c_{s,s',i,k}Q_v)}{\sin(\frac{d}{\lambda}c_{s,s',i,k})} \to 0$ as $(Q_h,Q_v) \to \infty$. Using this fact in (43), for large (Q_h,Q_v) we have

$$\frac{\gamma_{s,s',r,p}}{Q} \approx 0$$
, Large (Q_h, Q_v) . (46)

$\begin{array}{c} \text{APPENDIX C} \\ \text{EXPRESSION FOR } \gamma_{s,s,r,r}/Q \end{array}$

From (24) we have

$$\frac{\gamma_{s,s,r,r}}{Q} = \sum_{q=1}^{Q} \sum_{i=1}^{L_s} \left[\frac{|h_{q,s,i}|^2}{Q} \|\mathbf{a}_{s,i,r}\|^2 + \sum_{\substack{k=1\\k\neq i}}^{L_s} \frac{h_{q,s,i}h_{q,s,k}^*}{Q} \mathbf{a}_{s,i,r}^H \mathbf{a}_{s,k,r} \right]
\stackrel{(a)}{=} \sum_{i=1}^{L_s} |g_{s,i}|^2
+ \sum_{i=1}^{L_s} \sum_{\substack{k=1\\k\neq i}}^{L_s} \mathbf{a}_{s,i,r}^H \mathbf{a}_{s,k,r} \left\{ e^{j\pi \frac{d}{\lambda}((Q_h-1)b_{s,s,i,k}+(Q_v-1)c_{s,s,i,k})} \right.
g_{s,i}g_{s,k}^* \frac{\sin(\frac{d}{\lambda}b_{s,s,i,k}Q_h)}{\sin(\frac{d}{\lambda}c_{s,s,i,k}Q_v)} \frac{\sin(\frac{d}{\lambda}c_{s,s,i,k}Q_v)}{\sin(\frac{d}{\lambda}c_{s,s,i,k})} \right\}$$
(47)

where step (a) follows from (2) and $b_{s,s,i,k}, c_{s,s,i,k}$ are given by (44) with s'=s. In step (a) we have also used the fact that $\|\mathbf{a}_{s,i,r}\|^2=1$ (see (40)). Further, since the azimuthal and zenith angles for any two channel paths to a UT are not the same, for any $i\neq k$, at least one among $b_{s,s,i,k}$ or $c_{s,s,i,k}$ is not zero. Hence, as $(Q_h,Q_v)\to\infty$, the term $\frac{\sin(\frac{d}{\hbar}b_{s,s,i,k}Q_h)}{\sin(\frac{d}{\hbar}b_{s,s,i,k})}\frac{\sin(\frac{d}{\hbar}c_{s,s,i,k}Q_v)}{\sin(\frac{d}{\hbar}c_{s,s,i,k})}\to 0$ for all $i\neq k$. Using this fact in (47), for large (Q_h,Q_v) we have

$$\frac{\gamma_{s,s,r,r}}{Q} \approx \sum_{i=1}^{L_s} |g_{s,i}|^2, \quad \text{Large } (Q_h, Q_v). \tag{48}$$

APPENDIX D

Expression for $\gamma_{s,s,r,p}/Q$ $(r \neq p)$

From (24) we have

$$\begin{split} \frac{\gamma_{s,s,r,p}}{Q} &= \sum_{i=1}^{L_s} \left[\left(\sum_{q=1}^{Q} |h_{q,s,i}|^2 / Q \right) \mathbf{a}_{s,i,r}^H \mathbf{a}_{s,i,p} \right. \\ &+ \sum_{\substack{k=1\\k\neq i}}^{L_s} \left(\sum_{q=1}^{Q} h_{q,s,i} h_{q,s,k}^* / Q \right) \mathbf{a}_{s,i,r}^H \mathbf{a}_{s,k,p} \right] \\ &\stackrel{(a)}{=} \sum_{i=1}^{L_s} \sum_{\substack{k=1\\k\neq i}}^{L_s} \mathbf{a}_{s,i,r}^H \mathbf{a}_{s,k,p} \left[e^{j\pi \frac{d}{\lambda} ((Q_h - 1)b_{s,s,i,k} + (Q_v - 1)c_{s,s,i,k}) \right] \end{split}$$

$$g_{s,i} g_{s,k}^* \frac{\operatorname{sinc}(\frac{d}{\lambda} b_{s,s,i,k} Q_h)}{\operatorname{sinc}(\frac{d}{\lambda} b_{s,s,i,k})} \frac{\operatorname{sinc}(\frac{d}{\lambda} c_{s,s,i,k} Q_v)}{\operatorname{sinc}(\frac{d}{\lambda} c_{s,s,i,k})}$$
(49)

where step (a) follows from (2) and the fact that for any $p \neq r$, $\mathbf{a}_{s,i,r}^H \mathbf{a}_{s,i,p} = 0$ (see (41)). Further, since the azimuthal and zenith angles are not the same for any two channel paths to a UT, for any $i \neq k$, at least one among $b_{s,s,i,k}$ or $c_{s,s,i,k}$ is not zero. Hence, as $(Q_h,Q_v) \to \infty$, the term $\frac{\sin(\frac{d}{h}b_{s,s,i,k}Q_h)}{\sin(\frac{d}{h}b_{s,s,i,k})} \frac{\sin(\frac{d}{h}c_{s,s,i,k}Q_v)}{\sin(\frac{d}{h}c_{s,s,i,k})} \to 0 \text{ for all } i \neq k.$ Using this fact in (49), for large (Q_h,Q_v) we have

$$\frac{\gamma_{s,s,r,p}}{Q} \approx 0$$
, Large (Q_h, Q_v) . (50)

APPENDIX E PROOF OF THEOREM 2

We firstly find a good approximation to $C(\mathcal{P})$ in the large (Q_h, Q_v) regime with constant ρQ . From (24) we get

$$\frac{\mathbf{G}_{s,s}}{Q} = \sum_{q=1}^{Q} \sum_{i=1}^{L_s} \left(\frac{|h_{q,s,i}|^2}{Q} \mathbf{A}_{s,i} \mathbf{A}_{s,i}^H + \sum_{\substack{k=1\\k \neq i}}^{L_s} \frac{h_{q,s,i} h_{q,s,k}^*}{Q} \mathbf{A}_{s,i} \mathbf{A}_{s,k}^H \right)$$

$$\stackrel{(a)}{=} \sum_{i=1}^{L_s} \frac{\sum\limits_{q=1}^{Q} |h_{q,s,i}|^2}{Q} \mathbf{I} + \sum_{i=1}^{L_s} \sum_{\substack{k=1 \ Q}}^{L_s} \frac{\sum\limits_{q=1}^{Q} h_{q,s,i} h_{q,s,k}^*}{Q} \mathbf{A}_{s,i} \mathbf{A}_{s,k}^H$$

$$\stackrel{(b)}{\approx} \left(\sum_{i=1}^{L_s} |g_{s,i}|^2 \right) \mathbf{I} , \text{ Large } (Q_h, Q_v)$$
 (51)

where step (a) follows from the expression for $h_{q,s,i}$ in (2) and the fact that $\mathbf{A}_{s,i}\mathbf{A}_{s,i}^H=\mathbf{I}$ (see (42)). Step (b) follows from the fact that, for all $i\neq k$, $(\sum_{q=1}^Q h_{q,s,i}h_{q,s,k}^*/Q)\to 0$ as $(Q_h,Q_v)\to\infty$ (see (49) and the paragraph following it). Similarly, from (24) we also have

$$\frac{\mathbf{G}_{s,s'}}{Q} = \sum_{i=1}^{L_s} \sum_{k=1}^{L_{s'}} \frac{\sum_{q=1}^{Q} h_{q,s,i} h_{q,s',k}^*}{Q} \mathbf{A}_{s,i} \mathbf{A}_{s',k}^H$$

$$\approx \mathbf{0}, \text{ Large } (Q_h, Q_v). \tag{52}$$

where we have used the fact that $(\sum_{q=1}^{Q} h_{q,s,i} h_{q,s',k}^*/Q) \to 0$ as $(Q_h, Q_v) \to \infty$ (see (44) and the paragraph following (45)). Using the large (Q_h, Q_v) approximation for $\mathbf{G}_{s,s'}/Q$ from (52) and the expression for η from (17), we get

$$\frac{E_T}{\eta N_o} \sum_{\substack{s'=1, \ s' \neq s}}^K \mathbf{G}_{s,s'} \mathbf{G}_{s,s'}^H = \frac{E_T Q}{\frac{\eta}{Q} N_o} \sum_{\substack{s'=1, \ s' \neq s}}^K \frac{\mathbf{G}_{s,s'}}{Q} \frac{\mathbf{G}_{s,s'}^H}{Q}$$

$$\stackrel{(a)}{=} \frac{\rho Q}{\sum_{\tilde{s}=1}^K \sum_{i=1}^{L_{\tilde{s}}} \beta_{\tilde{s},i}} \sum_{\substack{s'=1, \ s' \neq s}}^K \frac{\mathbf{G}_{s,s'}}{Q} \frac{\mathbf{G}_{s,s'}^H}{Q}$$

$$\approx$$
 0, Large (Q_h, Q_v) and constant ρQ

where step (a) follows from (27) and the last step follows from the fact that ρQ is kept constant with increasing (Q_h,Q_v) . Using (51) and (53) in (25) we get the following large (Q_h,Q_v) with

constant ρQ approximation for $C_s(\mathcal{P})$ as

$$C_{s}(\mathcal{P}) \stackrel{(a)}{\approx} \frac{1}{MN \left(1 + \frac{\tau_{max}}{NT}\right)} \log_{2} \left| \mathbf{I} + \frac{MN(\rho Q)}{\eta/Q} \frac{\mathbf{G}_{s,s}}{Q} \frac{\mathbf{G}_{s,s}^{H}}{Q} \right|$$

$$\stackrel{(b)}{=} \frac{1}{MN \left(1 + \frac{\tau_{max}}{NT}\right)} \sum_{r=1}^{MN} \log_{2} \left(1 + \frac{\rho Q}{\frac{\eta/Q}{MN}} \left(\sum_{i=1}^{L_{s}} |g_{s,i}|^{2}\right)^{2}\right)$$

$$\stackrel{(c)}{\approx} \frac{1}{MN \left(1 + \frac{\tau_{max}}{NT}\right)} \sum_{r=1}^{MN} \log_{2} \left(1 + \frac{\rho Q \left(\sum_{i=1}^{L_{s}} |g_{s,i}|^{2}\right)^{2}}{\sum_{i=1}^{K} \sum_{j=1}^{L_{s}} \beta_{\tilde{s},i}}\right)$$

where step (a) follows from (27) and (53). Step (b) follows from (51) and step (c) follows from the expression for η in (17). From the large Q (with constant ρ Q) approximation of $I_{s,r}$ in (31) of Corollary 1 we have

$$R_{s}(\mathcal{P}) \stackrel{(a)}{=} \frac{1}{MN\left(1 + \frac{\tau_{max}}{NT}\right)} \sum_{r=1}^{MN} I_{s,r}(\mathcal{P})$$

$$\stackrel{(b)}{\approx} \frac{1}{MN\left(1 + \frac{\tau_{max}}{NT}\right)} \sum_{r=1}^{MN} \log_{2} \left(1 + \frac{\rho Q\left(\sum_{i=1}^{L_{s}} |g_{s,i}|^{2}\right)^{2}}{\sum_{\tilde{s}=1}^{K} \sum_{i=1}^{L_{\tilde{s}}} \beta_{\tilde{s},i}}\right)$$

where step (a) follows from the first definition in (29) and step (b) follows from (31). From (55) and (54) it follows that in the large (Q_h,Q_v) regime (with constant ρQ), $C_s(\mathcal{P})\approx R_s(\mathcal{P})$. The proof then follows from using this fact in (26) and (30).

APPENDIX F OTFS CHANNEL ESTIMATION

In this section, we discuss OTFS channel estimation considered by us in the numerical section. The OTFS massive MIMO channel estimation discussed here in the following is suited for systems where the BS does not have accurate knowledge of the antenna array steering vector. It is noted that prior works on OTFS massive MIMO channel estimation assume the exact knowledge of the antenna array steering vector at the BS [16], [22], [23]. In the considered TDD system, each UT sends a pilot symbol on a single designated DDRE in the uplink OTFS frame dedicated for uplink pilot transmission. For example, the placement of K = 4 pilots for the 4 UTs is shown in Fig. 13 for M = 330, N = 4. In our simulations we have considered a maximum path delay of $au_{max}=4.7~\mu s$, due to which a pilot transmitted by a UT on the (k,l)=(0,0)-th DDRE will be received between the l=0-th and the $l=\lceil \tau_{max} M \Delta f \rceil = 24$ -th DDRE along the delay domain ($\Delta f = 1/T = 15$ KHz). If we consider a maximum Doppler shift of $\nu_{max} = 1600$ Hz, then the same pilot will be spread over almost all the DDREs along the Doppler domain.

In order that the received pilots for the K=4 UTs do not interfere with each other along the delay domain, we place the pilots for the UTs at an interval of $\lfloor M/4 \rfloor = 82$ DDREs along the delay domain (see Fig. 13). The pilots for the four UTs are placed on DDREs having different Doppler domain indices in order that the interference between the received pilots is even

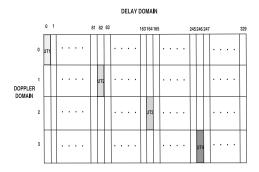


Fig. 13. Placement of uplink pilots in the DD domain. Pilots are transmitted by the UTs on the shaded DDREs.

smaller. Let the pilot for the s-th UT be located at the (k_s, l_s) -th DDRE, where $k_s = (s-1), l_s = (s-1)\lfloor M/4 \rfloor, s = 1, 2, 3, 4$. For the s-th UT we define its pilot region $\mathcal{R}_s = \{(k,l) \mid k = k_s, l-l_s \in [0\,,\,82]\}$ by the set of those DDREs where significant energy would be received only from the pilot transmitted by the s-th UT.

The DD domain pilot signal transmitted by the s-th UT is $x_s[k,l]=\sqrt{E_p}$ when $(k=k_s,l=l_s)$ and is zero for all other values of (k,l). Here E_p is the pilot energy. We assume power control for the uplink pilots, such that the pilot energy received from each UT is the same, i.e., E_p . The average uplink pilot power received from each UT is therefore $E_p/(NT)$. The noise power at each BS antenna in the communication bandwidth of $M\Delta f$ Hz is $M\Delta f N_o$. Therefore, the received pilot signal to noise ratio at the BS is $\rho_p \stackrel{\Delta}{=} E_p/(NTM\Delta f N_o) = E_p/(MNN_o)$ for each UT.

Let $\widehat{x}_q[k,l]$ denote the pilot signal received at the q-th BS antenna in the (k,l)-th DDRE, $k=0,1,\ldots,N-1,\ l=0,1,\ldots,M-1$. Further, let $\widehat{\mathbf{x}}_q\in\mathbb{C}^{MN\times 1}$ denote the vector of all symbols received on the MN DDREs at the q-th BS antenna, which is given by (57) as shown at the bottom of the next page. From the system model described in Section II it follows that the DD domain pilot signal received at the q-th BS antenna is given by

$$\widehat{\mathbf{x}}_{q} = \sum_{s=1}^{K} \mathbf{H}_{q,s} \mathbf{x}_{s} + \mathbf{w}_{q} = \sum_{s=1}^{K} \sum_{i=1}^{L_{s}} h_{q,s,i} \, \mathbf{A}_{s,i} \, \mathbf{x}_{s} + \mathbf{w}_{q}$$
(56)

where \mathbf{x}_s is the vector of DD domain pilot symbols transmitted by the s-th UT and is given by (57), shown at the see bottom of the next page. The AWGN in the (k,l)-th DDRE at the q-th BS antenna is denoted by $w_q[k,l], k=0,1,\ldots,N-1, l=0,1,\ldots,M-1$, and the vector of DD domain AWGN samples is denoted by \mathbf{w}_q .

Since, the s-th UT transmits an uplink pilot symbol only on the (k_s, l_s) -th DDRE, from (56) we have

$$\widehat{\mathbf{x}}_{q} = \sqrt{E_{p}} \sum_{s=1}^{K} \sum_{i=1}^{L_{s}} h_{q,s,i} \, \widetilde{\mathbf{a}}_{s,i}(l_{\tau_{s,i}}, \nu_{s,i}) + \mathbf{w}_{q}$$
 (58)

where $\tilde{\mathbf{a}}_{s,i}(l_{\tau_{s,i}},\nu_{s,i})\in\mathbb{C}^{MN\times 1}$ is the (k_sM+l_s+1) -th column of the matrix $\mathbf{A}_{s,i}$. The (KM+l+1)-th element of $\tilde{\mathbf{a}}_{s,i}(l_{\tau_{s,i}},\nu_{s,i})$ is $a_{s,i,k,l}[k_s,l_s]$ which is given by the expression for $a_{s,i,k,l}[k',l']$ in (39) with $k'=k_s$ and $l'=l_s$ (in (39) note the dependence on $l_{\tau_{s,i}}$ and $\nu_{s,i}$). The maximum likelihood (ML)

estimate of the channel path gains $\{h_{q,s,i}\}_{q=1,s=1,i=1}^{Q,K,L_s}$, the path delays $\{l_{\tau_{s,i}}\}_{s=1,i=1}^{K,L_s}$ and the Doppler shifts $\{\nu_{s,i}\}_{s=1,i=1}^{K,L_s}$ is then given by (59) as shown at the bottom of this page. The objective function in (59) can be further expressed as in (60).

$$\frac{1}{Q} \sum_{q=1}^{Q} \left\| \hat{\mathbf{x}}_{q} - \sqrt{E_{p}} \sum_{s=1}^{K} \sum_{i=1}^{L_{s}} h_{q,s,i} \, \tilde{\mathbf{a}}_{s,i} (l_{\tau_{s,i}}, \nu_{s,i}) \right\|^{2}$$

$$= \frac{1}{Q} \sum_{q=1}^{Q} \left\| \hat{\mathbf{x}}_{q} \right\|^{2} - \frac{2}{Q} \sqrt{E_{p}} \sum_{q=1}^{Q} \sum_{s=1}^{K} \sum_{i=1}^{L_{s}}$$

$$\Re \left[h_{q,s,i} \, \hat{\mathbf{x}}_{q}^{H} \, \tilde{\mathbf{a}}_{s,i} (l_{\tau_{s,i}}, \nu_{s,i}) \right]$$

$$+ E_{p} \sum_{s=1}^{K} \sum_{i=1}^{L_{s}} \underbrace{\left(\sum_{q=1}^{Q} |h_{q,s,i}|^{2} \right)}_{=|g_{s,i}|^{2} > 0, \sec(2)} \| \tilde{\mathbf{a}}_{s,i} (l_{\tau_{s,i}}, \nu_{s,i}) \|^{2}$$

$$+ E_{p} \sum_{s=1}^{K} \sum_{i=1}^{L_{s}} \sum_{\substack{i_{2}=1 \\ i_{2} \neq i_{1}}}^{L_{s}} \underbrace{\left(\sum_{q=1}^{Q} h_{q,s,i_{1}}^{*} h_{q,s,i_{2}} \right)}_{\rightarrow 0, \operatorname{as}(Q_{h}, Q_{v}) \to \infty}$$

$$\operatorname{see} (49) \operatorname{and para. after it}$$

$$\tilde{\mathbf{a}}_{s,i_{1}} (l_{\tau_{s,i_{1}}}, \nu_{s,i_{1}})^{H} \tilde{\mathbf{a}}_{s,i_{2}} (l_{\tau_{s,i_{2}}}, \nu_{s,i_{2}})$$

$$+ E_{p} \sum_{s_{1}=1}^{K} \sum_{s_{2}=1}^{K} \sum_{i_{1}=1}^{K} \sum_{i_{2}=1}^{L_{s_{2}}} \underbrace{\left(\sum_{q=1}^{Q} h_{q,s,i_{1}}^{*} h_{q,s,i_{2}} \right)}_{\rightarrow 0, \operatorname{as}(Q_{h}, Q_{v}) \to \infty}, \operatorname{see} (44) \operatorname{and para. after} (45)$$

$$\tilde{\mathbf{a}}_{s,i_{1}} (l_{\tau_{s,i_{1}}}, \nu_{s,i_{1}})^{H} \tilde{\mathbf{a}}_{s,i_{2}} (l_{\tau_{s,i_{2}}}, \nu_{s,i_{2}}).$$

From (60) we see that when the number of BS antennas is sufficiently large, a good approximation to the ML objective function is given by (61), as shown at the top of the next page.

Using the large antenna approximation of (61) in (59), the ML estimates are approximately given by (62), as shown at

the top of the next page. Here we have also used the fact that $\|\tilde{\mathbf{a}}_{s,i}(l_{T_{s,i}}, \nu_{s,i})\|^2 = 1$ (see (42)).

Due to the separation of the terms for each UT and each path, in the R.H.S. of (62), separate estimation of each UT's channel path gains, path delays and Doppler shifts can be performed. For the i-th path of the s-th UT, the proposed estimate of $l_{\tau_{s,i}}, \nu_{s,i}$ and $h_{q,s,i}, q=1,2,\ldots,Q$ is given by (63), as shown at the top of the next page.

For a given choice of $(l_{\tau_{s,i}}, \nu_{s,i})$, the choice of $h_{q,s,i}$ which maximizes the objective function in (63) is given by

$$\widehat{\widehat{h_{q,s,i}}}(l_{\tau_{s,i}}, \nu_{s,i}) = \frac{1}{\sqrt{E_p}} \, \tilde{\mathbf{a}}_{s,i}(l_{\tau_{s,i}}, \nu_{s,i})^H \widehat{\mathbf{x}}_q.$$
 (64)

Using this in (63) we further get (65), as shown at the top of the next page.

Due to the non-linear dependence of $\tilde{\mathbf{a}}_{s,i}(l_{\tau_{s,i}},\nu_{s,i})$ on $(l_{\tau_{s,i}},\nu_{s,i})$, it is difficult to derive a closed form expression for $\widehat{(l_{\tau_{s,i}},\hat{\nu_{s,i}})}$. Therefore, we propose the following method. Since $0 \leq l_{\tau_{s,i}} \leq (M-1)$ and $l_{\tau_{s,i}} \in \mathbb{Z}$, we firstly estimate the number of channel paths \widehat{L}_s for the s-th UT and the delay $l_{\tau_{s,i}}, i=1,2,\ldots,\widehat{L}_s$ for each path of the s-th UT by observing the distribution of the received energy in the pilot region \mathcal{R}_s dedicated for the s-th UT. Towards this end, for any l s.t. $(k,l) \in \mathcal{R}_s$ for some k, the energy received in the l-th DDRE along the delay domain is given by

$$\mathcal{E}_{s}[l] \stackrel{\Delta}{=} \frac{\sum\limits_{k \mid (k,l) \in \mathcal{R}_{s}} \sum\limits_{q=1}^{Q} |\widehat{x}_{q}[k,l]|^{2}}{Q}.$$
 (66)

The proposed estimate of the number of channel paths between the s-th UT and the BS is then given by the number of delay domain indices l for which $\mathcal{E}_s[l]$ exceeds a threshold \mathcal{E}_{th} , i.e.

$$\widehat{L}_{s} = \sum_{l \mid (k,l) \in \mathcal{R}_{s} \text{ for some } k} 1_{\varepsilon_{s}[l] > \varepsilon_{th}}$$

$$(67)$$

where $1_{\mathcal{E}_s[l]>\mathcal{E}_{th}}$ is one when $\mathcal{E}_s[l]>\mathcal{E}_{th}$ and is otherwise zero. The \widehat{L}_s estimated path delays $\widehat{l_{\tau_{s,i}}}, i=1,2,\ldots,\widehat{L}_s$ are then given by those indices l for which $\mathcal{E}_s[l]>\mathcal{E}_{th}$ and l is such that $(k,l)\in\mathcal{R}_s$ for some k. The threshold \mathcal{E}_{th} is chosen such that false detection of channel paths which do not exist is extremely rare. For the simulations presented in Section VI-A, we have considered $\mathcal{E}_{th}=4\,NN_o$, i.e., four times the mean value of $\mathcal{E}_s[l]$ in the presence of only AWGN (i.e., if no pilots are transmitted).

$$\widehat{\mathbf{x}}_{q} \stackrel{\triangle}{=} (\widehat{x}_{q}[0,0], \dots, \widehat{x}_{q}[0,M-1], \widehat{x}_{q}[1,0], \dots, \widehat{x}_{q}[1,M-1], \dots, \widehat{x}_{q}[N-1,0], \dots, \widehat{x}_{q}[N-1,M-1])^{T},$$

$$\mathbf{w}_{q} \stackrel{\triangle}{=} (w_{q}[0,0], \dots, w_{q}[0,M-1], w_{q}[1,0], \dots, w_{q}[1,M-1], \dots, w_{q}[N-1,0], \dots, w_{q}[N-1,M-1])^{T},$$

$$\mathbf{x}_{s} \stackrel{\triangle}{=} (x_{s}[0,0], \dots, x_{s}[0,M-1], x_{s}[1,0], \dots, x_{s}[1,M-1], \dots, x_{s}[N-1,0], \dots, x_{s}[N-1,M-1])^{T}$$
(57)

$$\widehat{\left(\{\widehat{h_{q,s,i}}\}_{q=1,s=1,i=1}^{Q,K,L_s}, \widehat{\{l_{\tau_{s,i}}\}_{s=1,i=1}^{K,L_s}, \{\widehat{\nu_{s,i}}\}_{s=1,i=1}^{K,L_s}\right)} \\
\stackrel{\triangle}{=} \arg \min_{\substack{\{h_{q,s,i}\}_{q=1,s=1,i=1,i=1}^{Q,K,L_s}, \{l_{\tau_{s,i}}\}_{s=1,i=1}^{K,L_s}, \{r_{q,s,i}\}_{s=1,i=1}^{K,L_s}, r_{q,s,i}\}} \widehat{\mathbf{x}}_{q} - \sqrt{E_p} \sum_{s=1}^{K} \sum_{i=1}^{L_s} h_{q,s,i} \, \tilde{\mathbf{a}}_{s,i} (l_{\tau_{s,i}}, \nu_{s,i}) \Big\|^{2}$$

$$\widehat{\mathbf{y}}_{s,i} \stackrel{K,L_s}{\models} \widehat{\mathbf{y}}_{s,i} \stackrel{K,L_s}{\models} \widehat{\mathbf{y}}_{s,i} \stackrel{K,L_s}{\models} \widehat{\mathbf{y}}_{s,i}}, \widehat{\mathbf{y}}_{s,i} \stackrel{K,L_s}{\models} \widehat{\mathbf{y}}_{s,i} \widehat{\mathbf{y}}_{s,i} \stackrel{K,L_s}{\models} \widehat{\mathbf{y}}_{s,i} \widehat{\mathbf$$

$$\sum_{q=1}^{Q} \left\| \widehat{\mathbf{x}}_{q} - \sqrt{E_{p}} \sum_{s=1}^{K} \sum_{i=1}^{L_{s}} h_{q,s,i} \, \widetilde{\mathbf{a}}_{s,i} (l_{\tau_{s,i}}, \nu_{s,i}) \right\|^{2} \approx \sum_{q=1}^{Q} \|\widehat{\mathbf{x}}_{q}\|^{2} - 2\sqrt{E_{p}} \sum_{s=1}^{K} \sum_{i=1}^{L_{s}} \sum_{q=1}^{Q} \Re \left[h_{q,s,i} \, \widehat{\mathbf{x}}_{q}^{H} \, \widetilde{\mathbf{a}}_{s,i} (l_{\tau_{s,i}}, \nu_{s,i}) \right] + E_{p} \sum_{s=1}^{K} \sum_{i=1}^{L_{s}} \sum_{q=1}^{Q} |h_{q,s,i}|^{2} \|\widetilde{\mathbf{a}}_{s,i} (l_{\tau_{s,i}}, \nu_{s,i})\|^{2}$$
(61)

$$\left(\{\widehat{h_{q,s,i}}\}_{q=1,s=1,i=1}^{Q,K,L_s}, \widehat{\{l_{\tau_{s,i}}\}_{s=1,i=1}^{K,L_s}}, \{\widehat{\nu_{s,i}}\}_{s=1,i=1}^{K,L_s}\right)$$

$$\approx \arg\max_{\substack{\{h_{q,s,i}\}_{q=1,s=1,i=1}^{Q,K,L_s}}} \sum_{i=1}^{S-1} \left[\sum_{q=1}^{Q} \left(2\sqrt{E_p} \Re\left[h_{q,s,i} \, \widehat{\mathbf{x}}_q^H \, \widetilde{\mathbf{a}}_{s,i} (l_{\tau_{s,i}}, \nu_{s,i}) \right] - E_p \, |h_{q,s,i}|^2 \right) \right]$$

$$\{l_{\tau_{s,i}}\}_{s=l,i=1}^{K,L_s}$$

$$(62)$$

$$\left(\{\widehat{\widehat{h_{q,s,i}}}\}_{q=1}^{Q}, \widehat{\widehat{l_{\tau_{s,i}}}}, \widehat{\widehat{\nu_{s,i}}}\right) \stackrel{\Delta}{=} \arg\max_{\substack{\{h_{q,s,i}\}_{q=1}^{Q} \\ l_{\tau_{s,i}}, \nu_{s,i}}} \left[\sum_{q=1}^{Q} \left(2\sqrt{E_{p}}\Re\left[h_{q,s,i}\,\widehat{\mathbf{x}}_{q}^{H}\,\widetilde{\mathbf{a}}_{s,i}(l_{\tau_{s,i}}, \nu_{s,i})\right] - E_{p}\,|h_{q,s,i}|^{2}\right)\right] \tag{63}$$

$$\widehat{\left(\widehat{l_{\tau_{s,i}}},\widehat{\nu_{s,i}}\right)} \stackrel{\triangle}{=} \arg\max_{l_{\tau_{s,i}},\nu_{s,i}} \left[\sum_{q=1}^{Q} \left(2\sqrt{E_p} \Re\left[\widehat{\widehat{h_{q,s,i}}}(l_{\tau_{s,i}},\nu_{s,i}) \widehat{\mathbf{x}}_{q}^{H} \widetilde{\mathbf{a}}_{s,i}(l_{\tau_{s,i}},\nu_{s,i}) \right] - E_p \left| \widehat{\widehat{h_{q,s,i}}}(l_{\tau_{s,i}},\nu_{s,i}) \right|^2 \right) \right] \\
= \arg\max_{l_{\tau_{s,i}},\nu_{s,i}} \sum_{q=1}^{Q} \left| \widetilde{\mathbf{a}}_{s,i}(l_{\tau_{s,i}},\nu_{s,i})^{H} \widehat{\mathbf{x}}_{q} \right|^2$$
(65)

Using (65) the proposed estimate for the Doppler shift of the *i*-th detected path of the *s*-th UT is given by

$$\widetilde{\nu_{s,i}} \stackrel{\Delta}{=} \arg \max_{-\nu_{max} \le \nu_{s,i} \le \nu_{max}} \sum_{q=1}^{Q} \left| \widetilde{\mathbf{a}}_{s,i} (\widetilde{l_{\tau_{s,i}}}, \nu_{s,i})^{H} \widehat{\mathbf{x}}_{q} \right|^{2}.$$
 (68)

In the absence of a closed-form expression for $\widetilde{\nu_{s,i}}$, for the simulations presented in Section VI-A we maximize the objective function in (68) over uniformly spaced 400 values of $\nu_{s,i}$ in the interval $[-\nu_{max}, \nu_{max}]$. Finally, just as in (64), the proposed estimate of $h_{q,s,i}$ for all $q=1,\ldots,Q,s=1,2,\ldots,K$ and $i=1,2,\ldots,\widehat{L}_s$ is given by

$$\widetilde{h_{q,s,i}} = \frac{1}{\sqrt{E_p}} \tilde{\mathbf{a}}_{s,i} (\widetilde{l_{\tau_{s,i}}}, \widetilde{\nu_{s,i}})^H \hat{\mathbf{x}}_q.$$
 (69)

Just as in (15), the proposed estimate of the DD domain channel between the s-th UT and the q-th BS antenna is

$$\widetilde{\mathbf{H}_{q,s}} \stackrel{\triangle}{=} \sum_{i=1}^{\widehat{L_s}} \widetilde{h_{q,s,i}} \widetilde{\mathbf{A}_{s,i}}$$
 (70)

where the element in the (kM+l+1)-th row and (k'M+l'+1)-th column of $\widetilde{\mathbf{A}_{s,i}} \in \mathbb{C}^{MN \times MN}$ is nothing but the expression for $a_{s,i,k,l}[k',l']$ in (39) with $l_{\tau_{s,i}}$ and $\nu_{s,i}$ replaced by their proposed estimates $\widetilde{l_{\tau_{s,i}}}$ and $\widetilde{\nu_{s,i}}$ respectively.

From (66), (67), (68), (69) and (70), it follows that the complexity of computing the proposed channel matrix estimates $\widetilde{\mathbf{H}}_{q,s}, q = 1, 2, \ldots, Q$ for a particular UT is $O(Q\widehat{L}_sMN^2)$. Here we have also used the fact that the vector $\widetilde{\mathbf{a}}_{s,i}(\widehat{l}_{\tau_{s,i}}, \widetilde{\nu_{s,i}})$ has only N non-zero entries (see the expression for $a_{s,i,k,l}[\cdot,\cdot]$ in (39)). As the DD domain channel matrix $\mathbf{H}_{q,s}$ has MN^2 non-zero entries, there are QMN^2 non-zero entries in all the Q channel

matrices $\mathbf{H}_{q,s}, q = 1, 2, \dots, Q$ for a given UT. Therefore, the complexity of estimating each non-zero entry is only $O(\widehat{L_s})$ (i.e., independent of (Q, M, N)).

REFERENCES

- R. Hadani, S. Rakib, M. Tsatsanis, A. Monk, A. J. Goldsmith, and A. F. Molisch, "Orthogonal time frequency space modulation," *IEEE Wireless Comm. Netw. Conf.*, Mar. 2017, pp. 1–6.
- [2] A. Monk, R. Hadani, M. Tsatsanis, and S. Rakib, "OTFS—Orthogonal time frequency space: A novel modulation meeting 5G high mobility and massive MIMO challenges," Aug. 2016, arXiv:1608.02993.
- [3] R. Hadani and A. Monk, "OTFS: A new generation of modulation addressing the challenges of 5G," Feb. 2018, arXiv:1802.02623.
- [4] S. K. Mohammed, "Derivation of OTFS modulation from first principles," *IEEE Trans. Veh. Technol.*, to be published, doi: 10.1109/TVT.2021.3069913.
- [5] P. Raviteja, K. T. Phan, Y. Hong, and E. Viterbo, "Interference cancellation and iterative detection for orthogonal time frequency space modulation," *IEEE Trans. Wireless Comm.*, vol. 17, no. 10, pp. 6501–6515, Oct. 2018.
- [6] R. Raviteja, K. T. Phan, Q. Jin, Y. Hong, and E. Viterbo, "Low-complexity iterative detection for orthogonal time frequency space modulation," in *Proc. IEEE Wireless Comm. Netw. Conf.*, Apr. 2018, pp. 1–6.
- [7] L. Li, Y. Liang, P. Fan, and Y. Guan, "Low complexity detection algorithms for OTFS under rapidly time-varying channel," in *Proc. IEEE Veh. Technol. Conf.*, Apr.–May 2019, pp. 1–5.
- [8] L. Gaudio, M. Kobayashi, G. Caire, and G. Colavolpe, "On the effectiveness of OTFS for joint radar parameter estimation and communication," *IEEE Trans. Wireless Commun.*, vol. 19, no. 9, pp. 5951–5965, Sep. 2020.
- [9] S. Tiwari, S. S. Das, and V. Rangamgari, "Low complexity MMSE receiver for OTFS," *IEEE Commun. Lett.*, vol. 23, no. 12, pp. 2205–2209, Dec. 2019.
- [10] M. K. Ramachandran and A. Chockalingam, "MIMO-OTFS in high-doppler fading channels: Signal detection and channel estimation," in *Proc. IEEE Glob. Commun. Conf.*, Kansas City, MO, USA, Dec. 2018, pp. 206–212.

- [11] W. Xu, T. Zou, H. Gao, Z. Bie, Z. Feng, and Z. Ding, "Low-complexity linear equalization for OTFS systems with rectangular waveforms," Nov. 2019, arXiv:1911.08133v1.
- [12] W. Yuan, Z. Wei, J. Yuan, and D. W. K. Ng, "A simple variational bayes detector for orthogonal time frequency space (OTFS) modulation," *IEEE Trans. Veh. Technol.*, vol. 69, no. 7, pp. 7976–7980, Jul. 2020.
- [13] IMT Vision Framework and Overall Objectives of the Future Deployment of IMT for 2020 and Beyond, Recommendation ITU-R M-2083-0, Sep. 2015. [Online]. Available: www.itu.int
- [14] E. G. Larsson, O. Edfors, F. Tufvesson, and T. L. Marzetta, "Massive MIMO for next generation wireless systems," *IEEE Commun. Mag.*, vol. 52, no. 2, pp. 186–195, Feb. 2014.
- [15] Y. Shan and F. Wang, "Low-complexity and low-overhead receiver for OTFS Via large-scale antenna array," May 2020, arXiv:2005.07910v1.
- [16] M. Li, S. Zhang, F. Gao, P. Fan, and O. A. Dobre, "A new path division multiple access for the massive MIMO-OTFS networks," *IEEE J. Sel. Areas Commun.*, vol. 39, no. 4, pp. 903–918, Apr. 2021.
- [17] T. Zemen, D. Löschenbrand, M. Hofer, C. Pacher, and B. Rainer, "Orthogonally precoded massive MIMO for high mobility scenarios," *IEEE Access*, vol. 7, pp. 132979–132990, Sep. 2019.
- [18] T. L. Marzetta, E. G. Larsson, H. Yang, and H. Q. Ngo, Fundamentals of Massive MIMO. Cambridge, U.K.: Cambridge Univ. Press, 2016.
- [19] W. C. Jakes, Jr., Microwave Mobile Communications. New York, NY, USA: Wiley, 1974.
- [20] P. A. Bello, "Characterization of randomly time-variant linear channels," IEEE Trans. Commun. Syst., vol. 11, no. 4, pp. 360–393, Dec. 1963.
- [21] R. Yin, X. Zhou, A. Wang, C. Zhong, C. Wu, and X. Chen, "Adaptive channel estimation and tracking for URA-based massive MIMO systems," *IEEE Access*, vol. 8, pp. 54213–54224, Mar. 2020.
- [22] W. Shen, L. Dai, J. An, P. Fan, and R. W. Heath, "Channel estimation for orthogonal time frequency space (OTFS) massive MIMO," *IEEE Trans. Signal Process.*, vol. 67, no. 16, pp. 4204–4217, Aug. 2019.
- [23] Y. Liu, S. Zhang, F. Gao, J. Ma, and X. Wang, "Uplink-aided high mobility downlink channel estimation over massive MIMO-OTFS system," *IEEE J. Sel. Areas Commun.*, vol. 38, no. 9, pp. 1994–2009, Sep. 2020.
- [24] P. Raviteja, Y. Hong, E. Viterbo, and E. Biglieri, "Practical pulse-shaping waveforms for reduced-cyclic-prefix OTFS," *IEEE Trans. Veh. Technol.*, vol. 68, no. 1, pp. 957–961, Jan. 2019.
- [25] D. N. C. Tse and P. Vishwanath, Fundamentals of Wireless Communication, Cambridge, U.K.: Cambridge Univ. Press, 2005.
- [26] T. M. Cover and J. A. Thomas, *Elements of Information Theory*. 2nd ed., Hoboken, NJ, USA: Wiley, 2006.
- [27] "Study on channel models for frequencies from 0.5 to 100 GHz," 3GPP Tech. Rep. TR 38.901 Release 16, Oct. 2019.
- [28] A. Pfadler, P. Jung, and S. Stanczak, "Mobility modes for pulse-shaped OTFS with linear equalizer," in *Proc. IEEE Glob. Commun. Conf.*, Dec. 2020, pp. 1–6.



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